



US009249693B2

(12) **United States Patent**
Warren et al.

(10) **Patent No.:** **US 9,249,693 B2**
(45) **Date of Patent:** ***Feb. 2, 2016**

(54) **OPPOSED PISTON DIESEL ENGINE**

(75) Inventors: **James C. Warren**, Fairfax, VA (US);
Dennis K. Scheer, Birmingham, MI
(US)

(73) Assignee: **WARREN ENGINE COMPANY,**
INC., Bluemont, VA (US)

(*) Notice: Subject to any disclaimer, the term of this
patent is extended or adjusted under 35
U.S.C. 154(b) by 1185 days.

This patent is subject to a terminal dis-
claimer.

(21) Appl. No.: **12/645,287**

(22) Filed: **Dec. 22, 2009**

(65) **Prior Publication Data**

US 2010/0170466 A1 Jul. 8, 2010

Related U.S. Application Data

(60) Provisional application No. 61/203,701, filed on Dec.
22, 2008, provisional application No. 61/180,108,
filed on May 20, 2009.

(51) **Int. Cl.**
F01L 7/00 (2006.01)
F01L 1/30 (2006.01)
F01L 7/02 (2006.01)
F02B 75/28 (2006.01)

(52) **U.S. Cl.**
CPC . **F01L 1/30** (2013.01); **F01L 7/029** (2013.01);
F02B 75/282 (2013.01); **F01L 2105/00**
(2013.01)

(58) **Field of Classification Search**
USPC 123/188.16, 190.1, 51 R, 51 AA, 51 BA,

123/51 BB, 51 BC, 51 BD, 188.2, 188.4,
123/90.1, 90.2, 90.21, 90.39, 90.41, 90.44,
123/58.1, 59.1, 59.3, 80 R, 81 C, 190.12,
123/190.13, 190.3, 190.4, 190.6, 190.7,
123/190.8, 190.9, 190.11, 190.14, 190.15,
123/190.2, 190.17, 59.2, 59.4, 80 BA,
123/80 BB, 80 C, 80 D, 80 DA, 81 R, 81 B,
123/81 D

See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

2,280,079	A *	4/1942	Pletcher et al.	123/51 R
4,098,238	A *	7/1978	Vallejos	123/81 B
5,351,657	A *	10/1994	Buck	123/43 C
5,690,069	A *	11/1997	Huwarts	123/190.2
7,004,120	B2 *	2/2006	Warren	123/43 R
7,779,795	B2 *	8/2010	Warren	123/51 R
2007/0017476	A1 *	1/2007	Zajac et al.	123/190.1
2007/0095320	A1 *	5/2007	Warren	123/162

* cited by examiner

Primary Examiner — Hung Q Nguyen

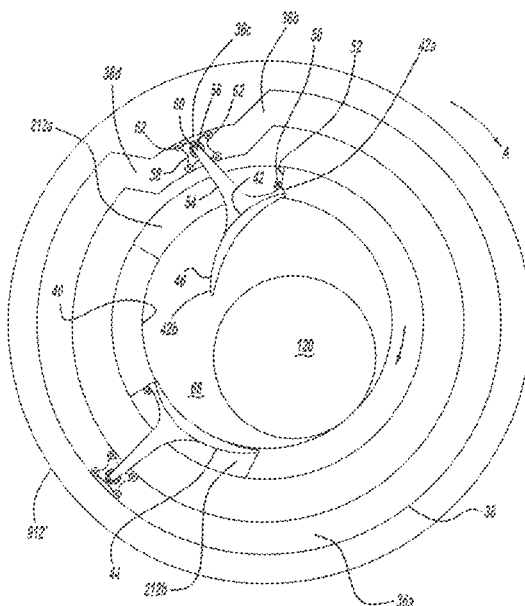
Assistant Examiner — Ruben Picon-Feliciano

(74) *Attorney, Agent, or Firm* — L.C. Begin & Associates,
PLLC

(57) **ABSTRACT**

An opposed piston engine includes a valve mechanism for
regulating fluid flow through an opening formed in a cylinder
of the engine. The mechanism includes a valve operatively
coupled to the cylinder so as to be rotatable to a first position
to seal the opening and to a second position to unseal the
opening, and at least one cam surface operatively coupled to
the cylinder so as to be movable with respect to the cylinder to
engage the valve so as to produce rotation of the valve.

20 Claims, 12 Drawing Sheets



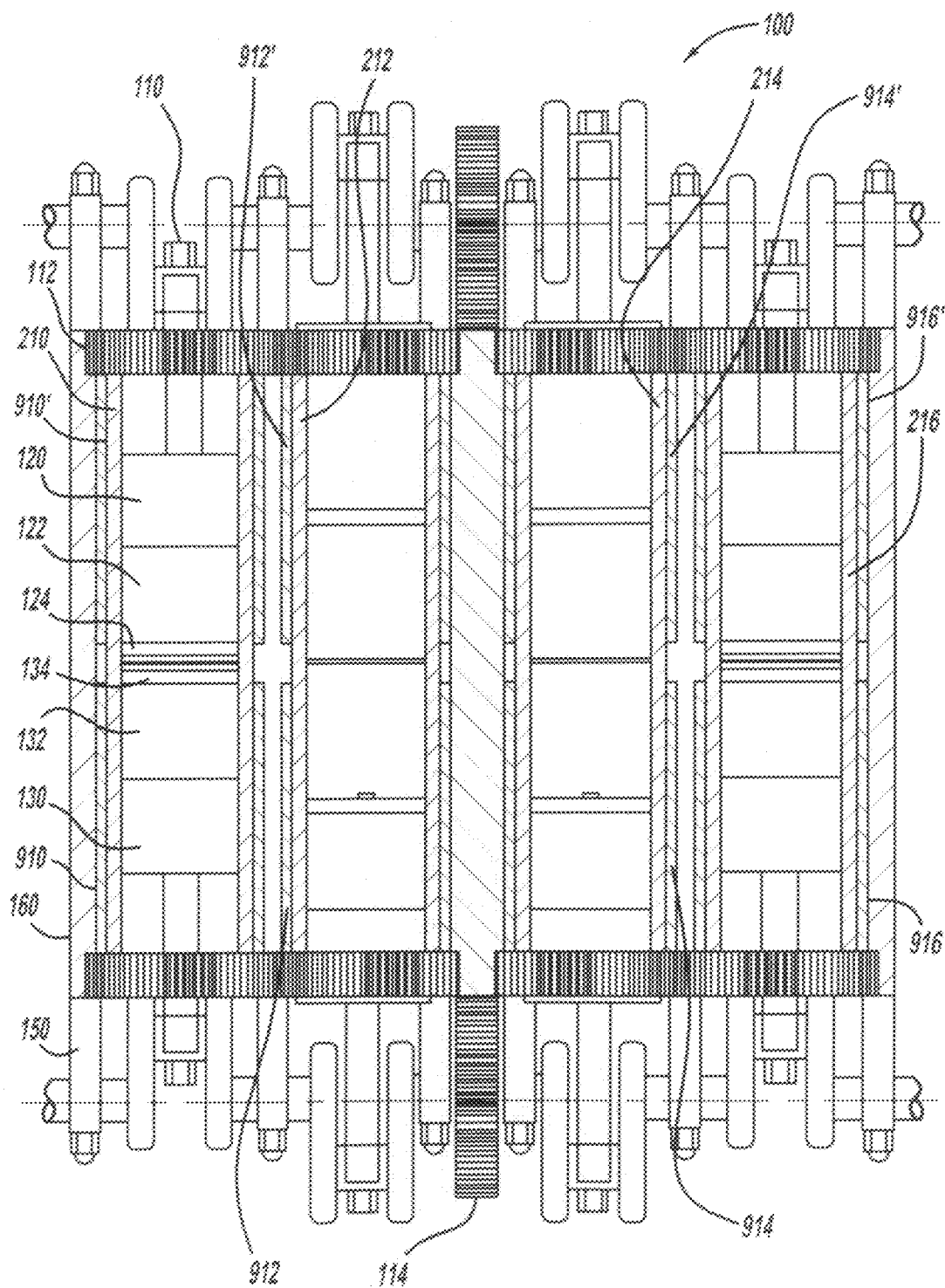


FIG - 1

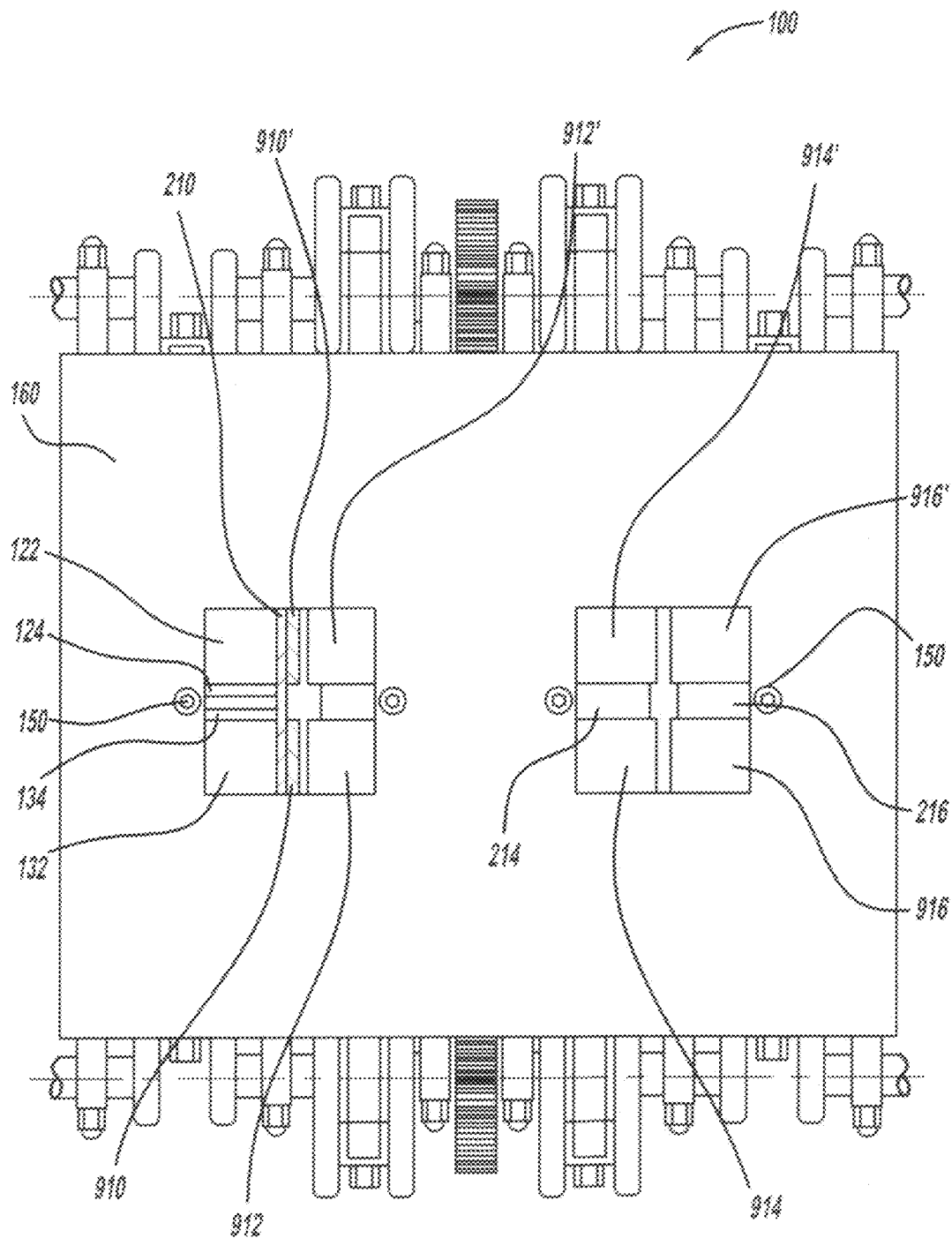


FIG - 2

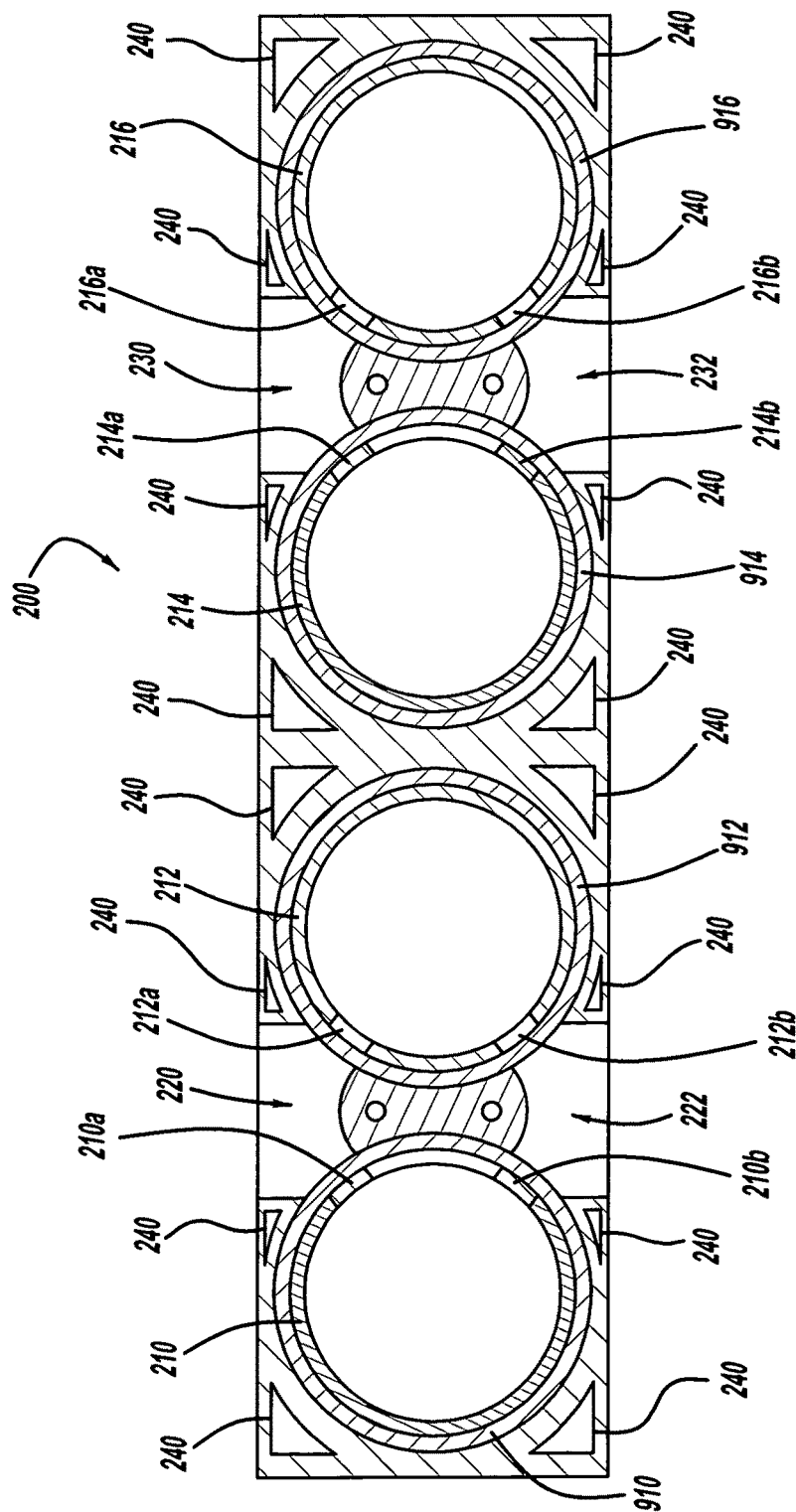


FIG - 3

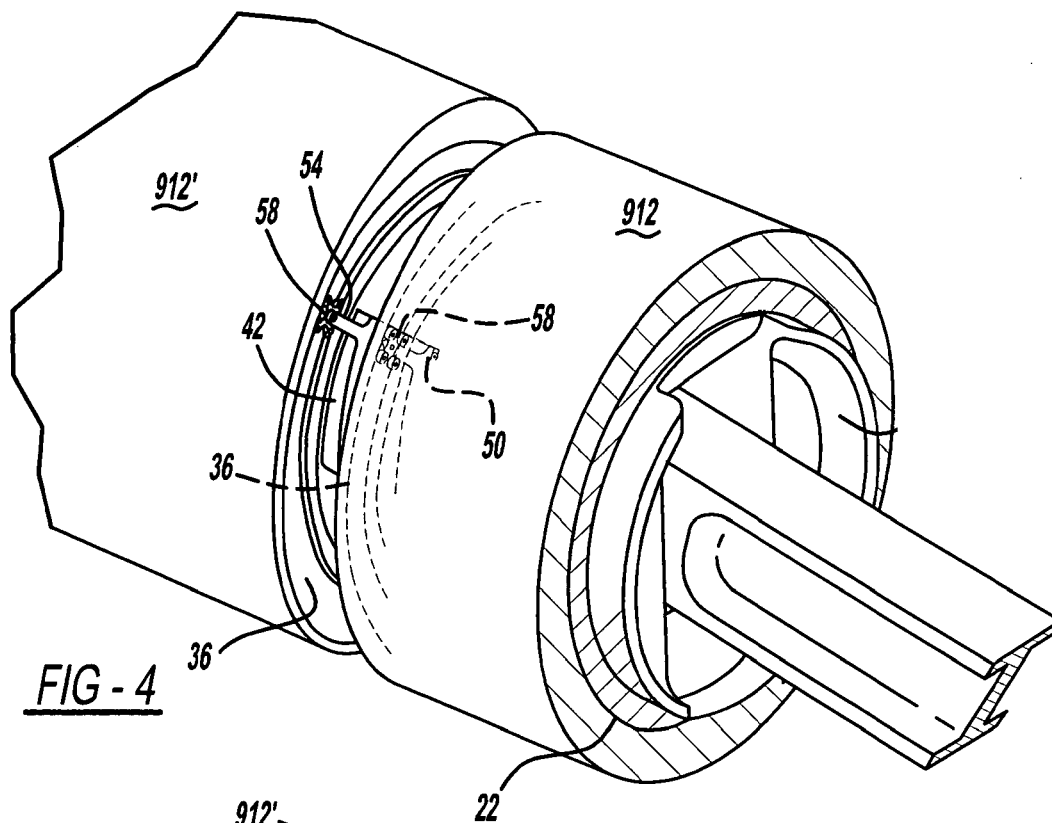


FIG - 4

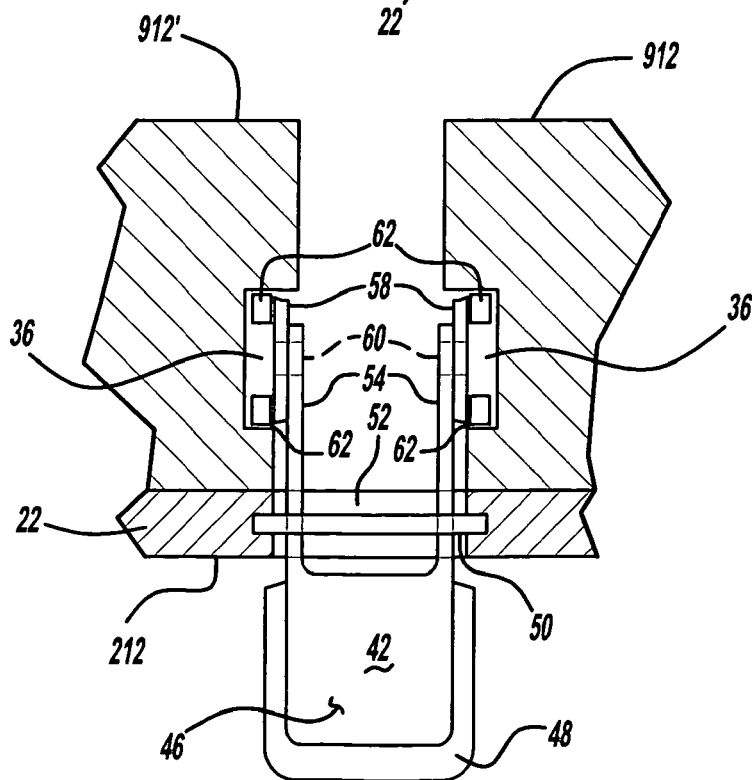


FIG - 5

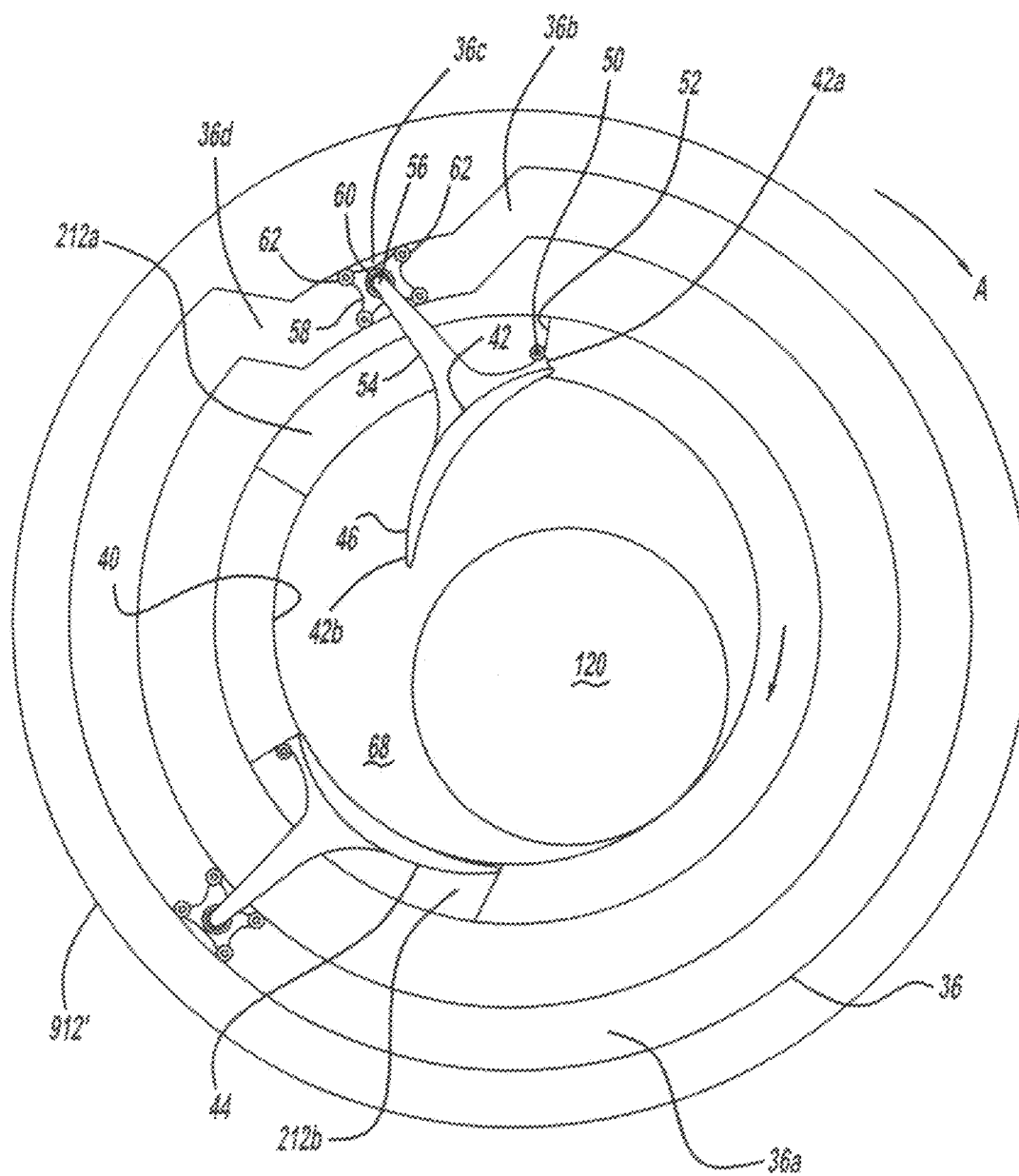


FIG - 6

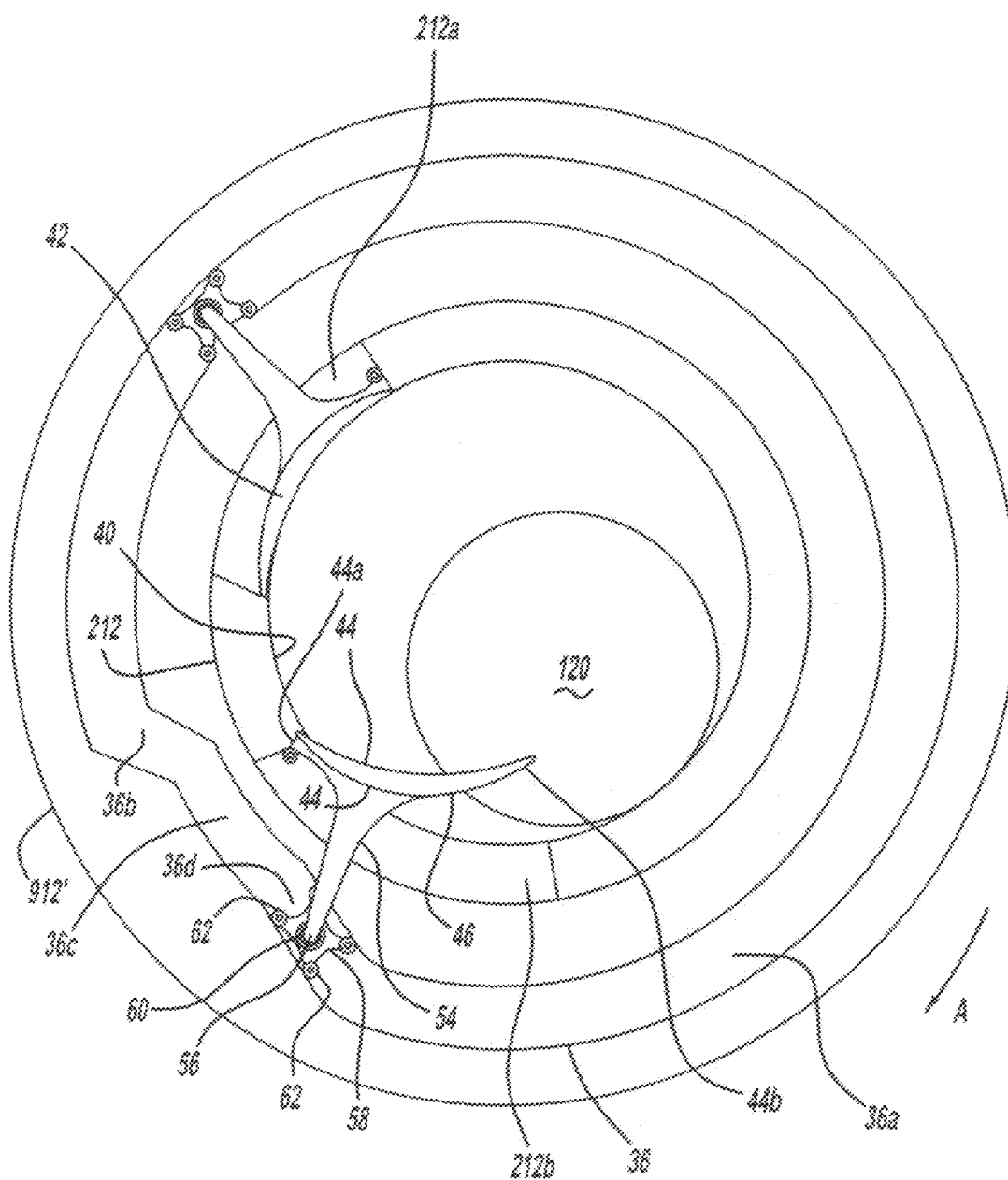


FIG - 7

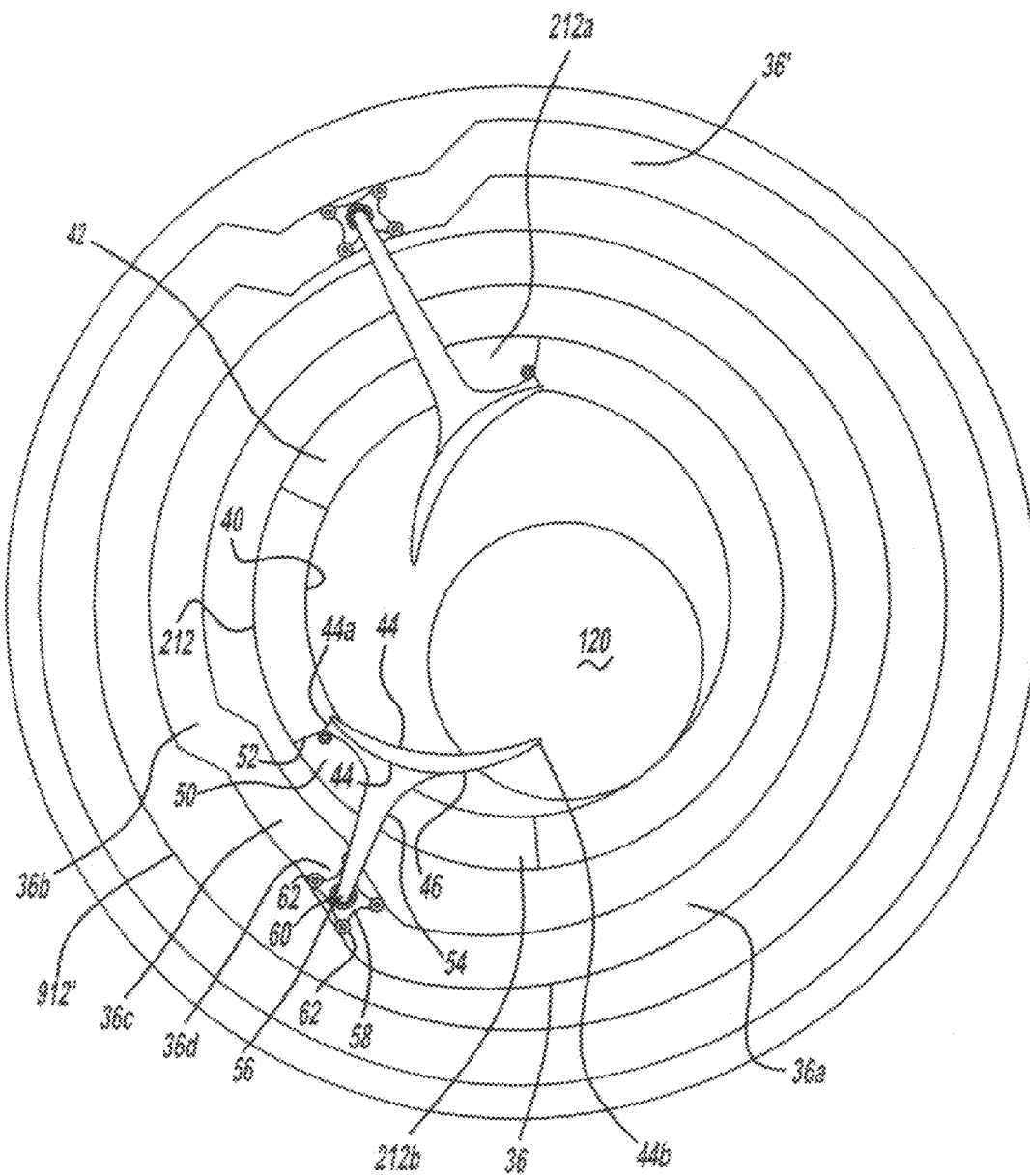


FIG - 8

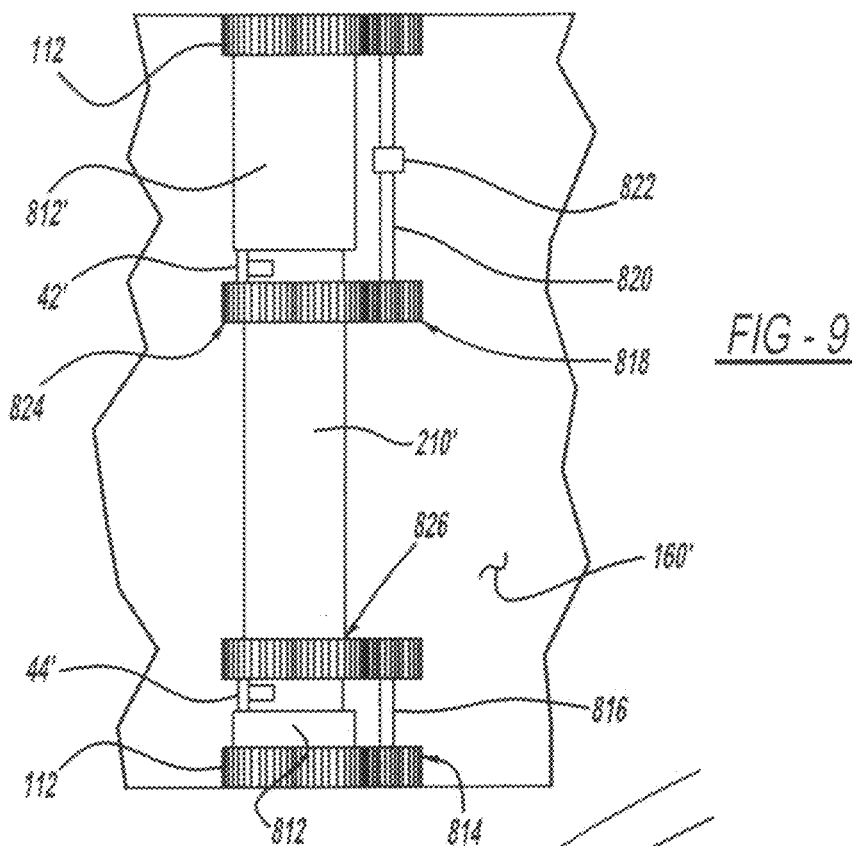
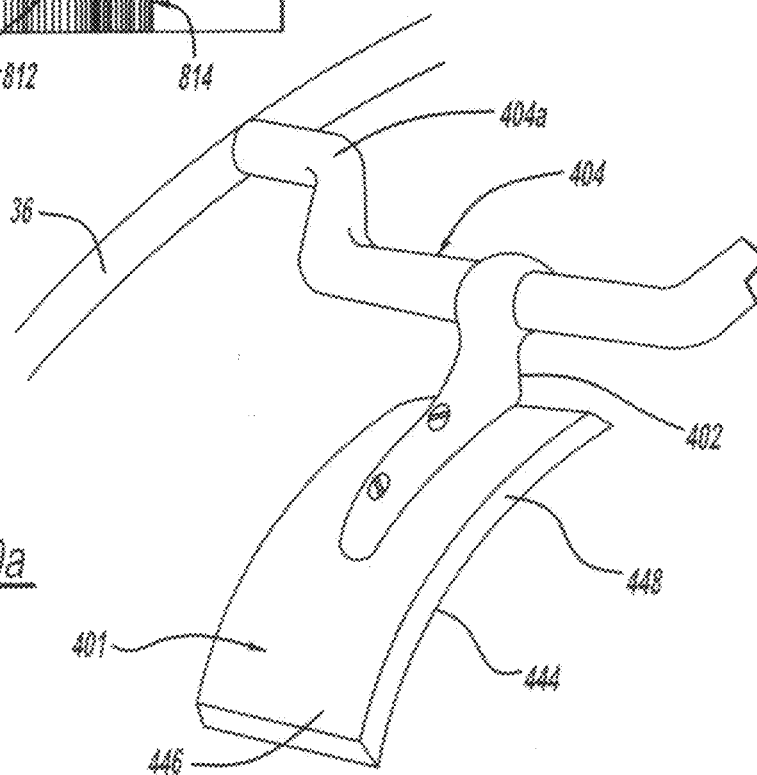


FIG - 10a



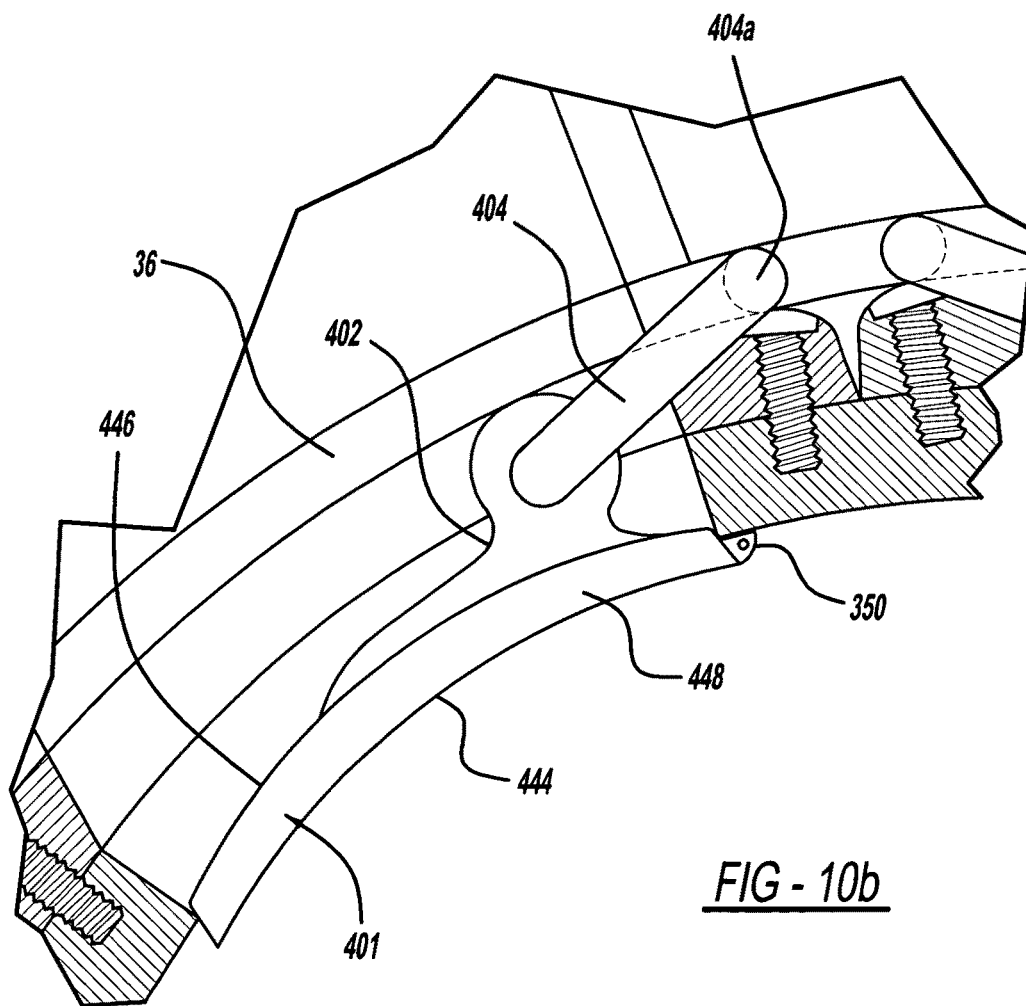
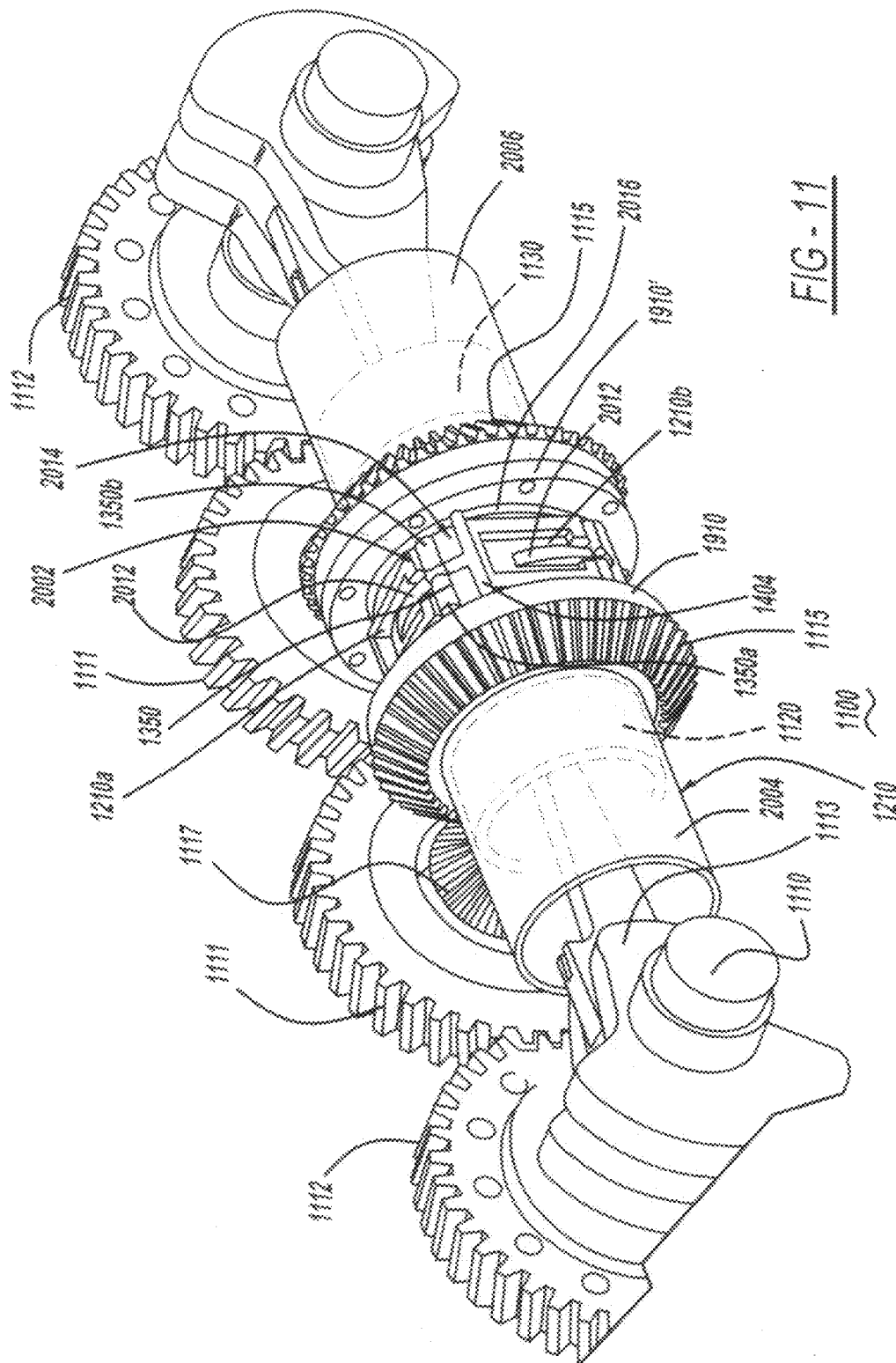
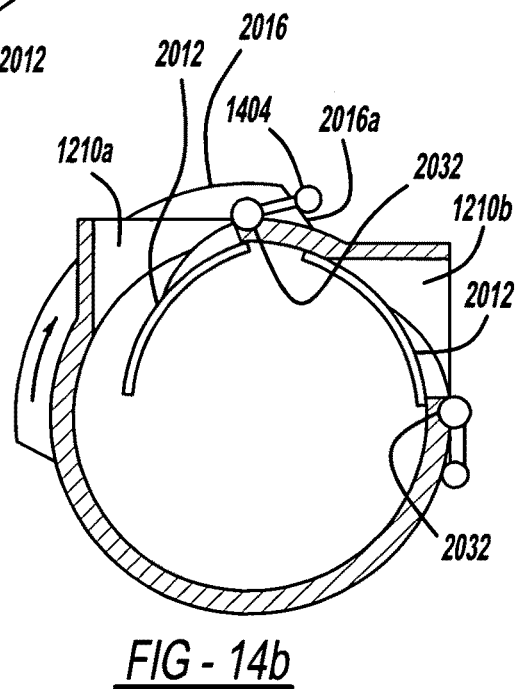
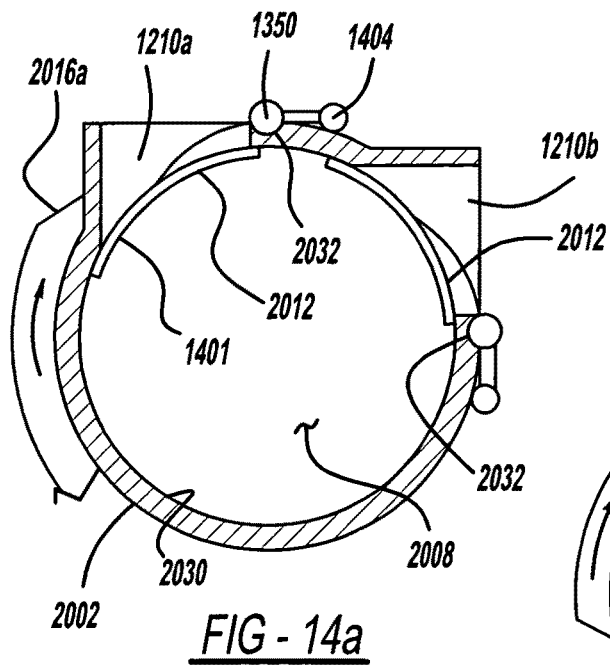
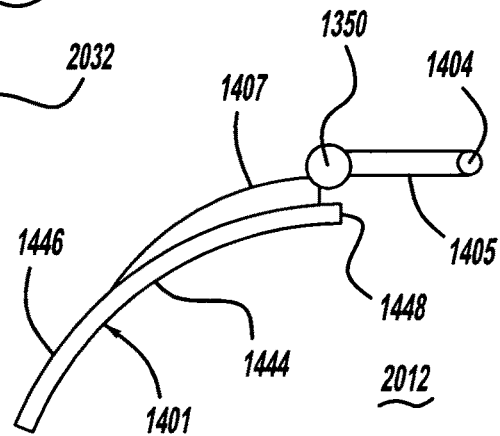
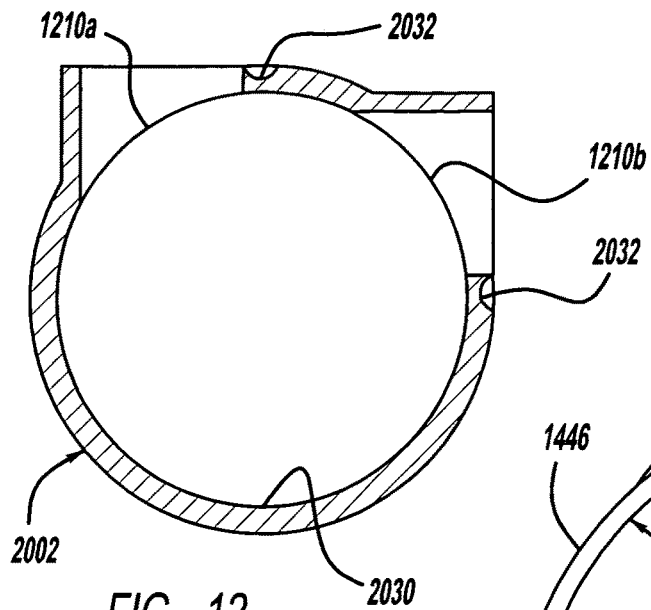
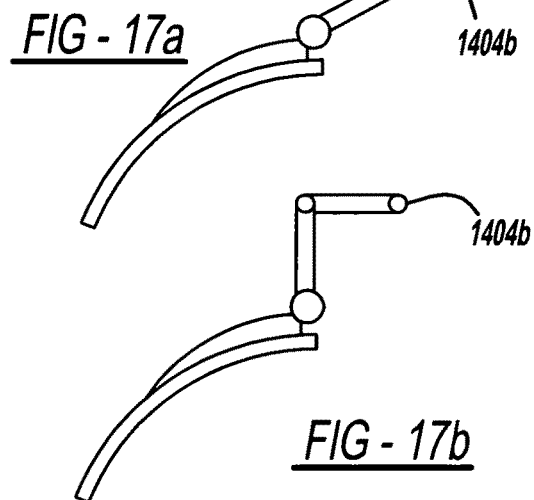
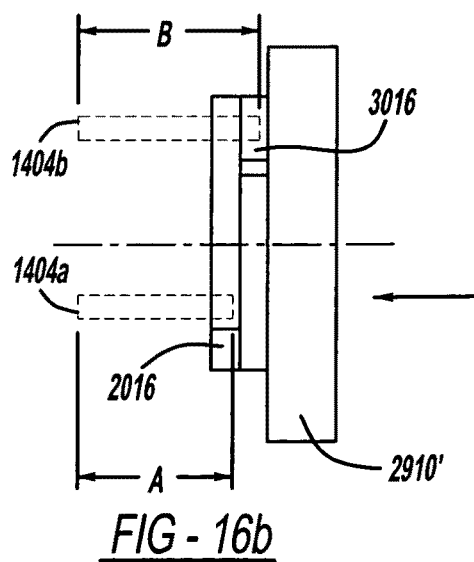
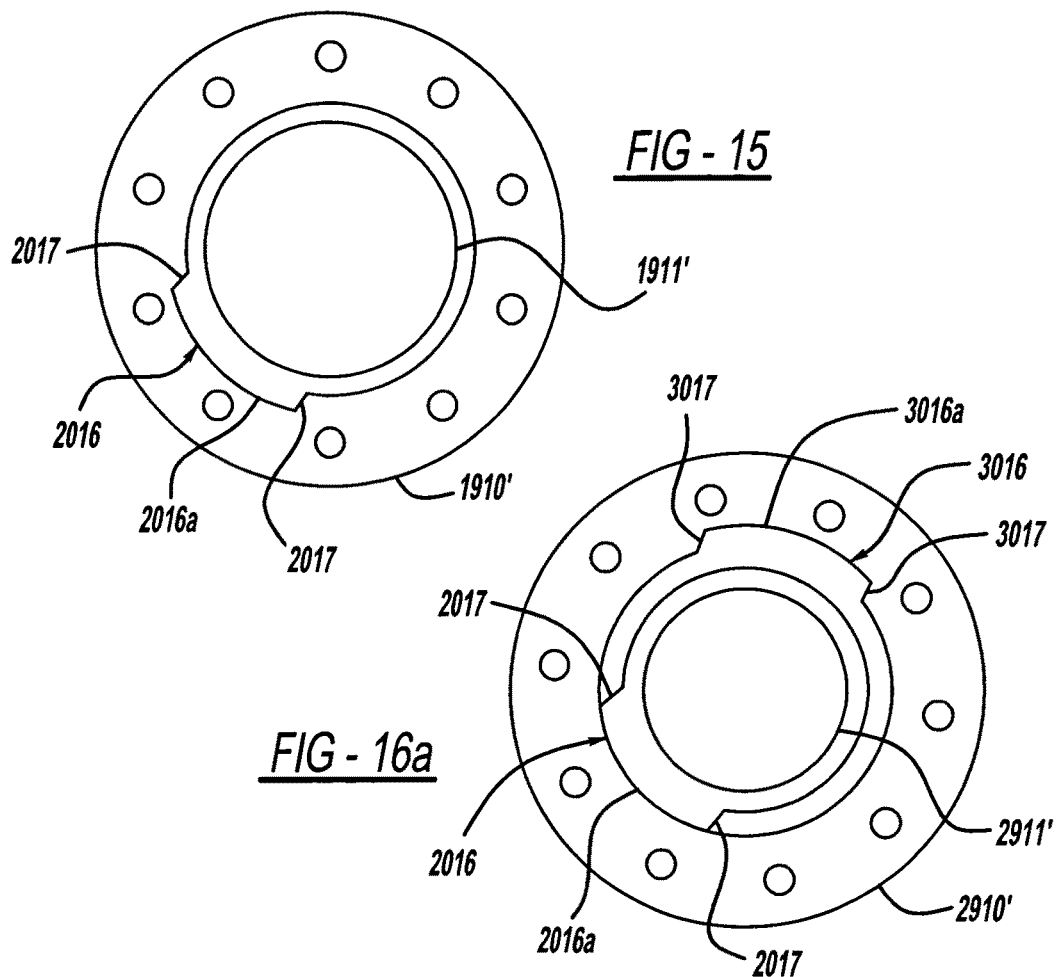


FIG - 10b



1963





1

OPPOSED PISTON DIESEL ENGINE**CROSS REFERENCE TO RELATED APPLICATIONS**

This application claims the benefit of provisional application Ser. No. 61/203,701, filed on Dec. 22, 2008, and of provisional application Ser. No. 61/180,108 filed on May 20, 2009, both incorporated herein by reference.

BACKGROUND OF THE INVENTION

The embodiments of the present invention relate to engines and, more particularly, to an opposed piston diesel engine.

SUMMARY OF THE INVENTION

In one aspect of embodiments of the present invention, an opposed piston engine is provided including a valve mechanism for regulating fluid flow through an opening formed in a cylinder of the engine. The mechanism includes a valve operatively coupled to the cylinder so as to be rotatable to a first position to seal the opening and to a second position to unseal the opening, and at least one cam surface operatively coupled to the cylinder so as to be movable with respect to the cylinder to engage the valve so as to produce rotation of the valve.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a cross-sectional view of an example of an opposed piston diesel engine according to the present invention.

FIG. 2 is a top view of the opposed piston diesel engine shown in FIG. 1.

FIG. 3 is a cross sectional view of an example of a block of an opposed piston diesel engine according to the present invention.

FIG. 4 is a broken away perspective view of the center of a single cylinder assembly of an opposed piston diesel engine, providing further details of the valve mechanism.

FIG. 5 is an elevation view in section through the central cylinder wall forming one side of the combustion chamber of the engine, showing further details of the valve assembly.

FIG. 6 is a cross-sectional view across a single combustion chamber of the engine, showing the rotation of a sleeve and resulting actuation of the valve during the intake portion of the diesel engine cycle.

FIG. 7 is a cross-sectional view across a single combustion chamber of the engine, showing the rotation of a sleeve and resulting actuation of the valve during the exhaust portion of the diesel engine cycle.

FIG. 8 is a cross-sectional view across a single combustion chamber of an alternative embodiment of the engine.

FIG. 9 is a cross-sectional view an exemplary cylinder and sleeve arrangement of an opposed piston diesel engine in accordance with an alternative embodiment of the present invention.

FIGS. 10a-10b show views of a valve mechanism in accordance with an alternative embodiment of the present invention.

FIG. 11 is a perspective view of a diesel engine cylinder assembly incorporating a valve mechanism in accordance with another embodiment of the present invention.

FIG. 12 is a cross-sectional view of a portion of a valve block incorporated in the embodiment shown in FIG. 11.

2

FIG. 13 is a side view of a valve incorporated in the embodiment shown in FIG. 11.

FIGS. 14a and 14b are cross-sectional views of a portion of the cylinder assembly shown in FIG. 11, showing operation of one of the valves incorporated therein.

FIG. 15 shows a rotatable sleeve in accordance with an embodiment of the present invention.

FIG. 16a is a plan view of a rotatable sleeve in accordance with an alternative embodiment of the present invention.

FIG. 16b is a side view of the sleeve shown in FIG. 16a.

FIGS. 17a-17b show valve configurations in accordance with alternative embodiments of the present invention.

DETAILED DESCRIPTION

Similar reference characters denote corresponding features throughout the attached drawings.

Referring to the drawings, an opposed piston diesel engine according to one embodiment of the present invention is shown in FIGS. 1-3. The arrangement shown is similar to embodiments of an opposed piston internal combustion engine described in U.S. Pat. No. 7,004,120, incorporated herein by reference. The embodiment 100 of the opposed piston diesel engine shown in FIGS. 1-3 is a four-cycle or four-stroke engine and while it is illustrated with four cylinders 210, 212, 214, and 216, any number of cylinders may be utilized depending on the amount of power desired to be produced by the engine 100. In addition, the structural arrangements and operating principles described herein may alternatively be applied to a two-stroke engine.

Referring to FIG. 1, each cylinder 210, 212, 214, and 216 of the engine forms (in conjunction with opposed pistons 120 and 130 disposed within the cylinder) a combustion chamber for the air-fuel combustion reaction. Each cylinder is associated with a respective pair of rotating outer sleeves 910, 910', 912, 912', 914, 914', and 916, 916' (e.g., sleeves 910 and 910' enclose cylinder 210 in FIG. 1), FIG. 1 shows rotating sleeves 912, 912' associated with cylinder 212, sleeves 914, 914' associated with cylinder 214, and sleeves 916, 916' associated with cylinder 216. An engine block or cylinder case 160 of the engine encloses the cylinder assemblies and opposed pistons. Each sleeve has camming surfaces formed in end portions thereof for purposes described in greater detail below. Each cylinder is also associated with a pair of connecting rods 110, a pair of opposing gears 112, opposing first and second pistons 120 and 130 that are each interconnected with a connecting rod 112, first and second opposing piston caps 124 and 134, and a pair of bearing caps 150. Optional first and second opposing cylindrical spacers 122 and 132 may be affixed to respective ones of the opposed pistons for purposes described below.

A gear 112 is attached to each end of an associated rotating sleeve and is driven by a gear 114 sharing the same axis as the associated crankshaft (not shown), to rotate the sleeve. Each associated crankshaft is configured to provide predetermined stroke lengths to the first and second pistons 120 and 130 residing within each cylinder. The opposed first and second pistons 120 and 130 may be of a relatively standard design, and have predetermined lengths and predetermined diameters.

Cylinders 210, 212, 214, 216 reside within respective outer sleeves 910, 910', 912, 912', 914, 914', and 916, 916' as shown in FIG. 1. Cylinders 210, 212, 214, 216 are also stationary with respect to the rotating sleeves. The gears 112 are configured to rotate each associated sleeve at a speed of one half crank speed, and each sleeve has a predetermined length. The sleeves of each pair of sleeves associated with an individual

cylinder rotate in conjunction with each other, at the same speed and in the same direction. Sleeve or plain bearings (not shown) or any other suitable bearings may be positioned between the cylinders and their respective sleeves to facilitate rotation of the sleeves with respect to the cylinders. Similarly, sleeve or plain bearings (not shown) or any other suitable bearings may be positioned between the rotating sleeves and the engine block **160** to facilitate rotation of the sleeves with respect to the engine block **160**. One source of suitable bearings for this application is GGB Bearings of Thorofare, N.J.

Referring to the arrangement within cylinder **210** of FIG. **1** as exemplary, optional first and second cylindrical spacers **122** and **132** may be affixed to the faces of the associated pistons **120** and **130**. The optional spacers **122** and **132** are not necessary but may be utilized to provide correct piston lengths for controlling spacing between the piston faces, thereby providing a means for adjusting the compression ratio and generally providing a predetermined degree of compression for heating intake air to facilitate combustion of a fuel injected or otherwise inserted into the combustion chamber. The piston lengths are geometrically determined in accordance with the piston stroke length and the lengths of apertures (described below) formed in the cylinders through which flow exhaust gases and air for combustion.

Referring again to cylinder **210** of FIG. **1**, first and second piston caps **124** and **134** are attached to faces of associated ones of pistons **120** and **130** (or to associated optional cylindrical spacers **122** and **132** in an embodiment where spacers are used). In one embodiment, each piston cap **124** and **134** is formed from a sandwich of two sheets of carbon fiber with a ceramic center. The piston caps **124** and **134** which are exposed to the combustion event are slightly concave in form so that when the two piston caps **124** and **134** meet in the center of the cylinder they form a somewhat spherical combustion chamber. Only the ceramic cores of the piston caps **124** and **134** actually come into contact with the stationary cylinder wall. A bearing cap **150** is mounted on each end of each rotating cylinder.

The piston should have a length from the fire ring to the cap suitable for keeping the piston rings out of the aperture. The optional spacers **122** and **132**, and piston caps **124** and **134** each have a diameter roughly equal to the interior of the associated cylinder, and may be made of carbon fiber, ceramic, or any other suitable material to aid in minimizing thermal inefficiencies during engine operation.

An external view of the opposed piston diesel engine **100** is shown in FIG. **2**, illustrating the block **160** itself with the intake plenums exposed. In FIGS. **1** and **2**, the first and second pistons **122** and **134** in the far left cylinder **210** are at the apex of their stroke, at which they would not be exposed during the actual operation of the engine **100**. An exemplary fuel injector **150** is shown for providing fuel to cylinder **210** at an appropriate point in the diesel engine cycle, as is known in the art.

A cross section of an engine block **200** showing two intake plenums **220** and **230**, and two associated exhaust plenums **222** and **232** is illustrated in FIG. **3**. Cooling channels **240** are also illustrated. Two cylinders **210** and **212** share a common intake and exhaust runner. In the embodiment shown in FIG. **3**, each runner, after branching off from the plenum, extends about sixty degrees along the outside diameter of the outer cylinder and is equal in length to the combined stroke lengths of both pistons. Various other conventional components of a diesel engine, e.g., cooling system, mechanical fasteners, etc., are not shown in the drawings in order to provide greater clarity for the inventive features shown therein.

Referring to FIG. **3**, each of cylinders **210**, **212**, **214**, **216** has a pair of apertures or valve ports formed therealong and

positioned so as to enable fluid communication between an interior of the cylinder and the associated intake and exhaust runners. Only the apertures formed along cylinder **210** will be described for simplicity. However, it will be understood that cylinders **212**, **214**, and **216** incorporate similar features arranged so as to facilitate execution of the diesel engine cycle described herein.

Referring to cylinder **210** of FIG. **3**, the cylinder includes a pair of apertures **210a** and **210b** formed therein, each aperture being aligned with a corresponding one of intake plenum **220** and exhaust plenum **222**. In the embodiment shown in FIG. **3**, apertures **210a** and **210b** are angularly spaced apart approximately 90° and each encompasses an arc of approximately 60°. However, other aperture sizes and angular arrangements may be used according to the requirements of a particular application. In addition, each aperture is associated with a respective valve mechanism (not shown in FIG. **3**) which is actuated responsive to the portion (i.e., intake, compression, power, or exhaust) of the engine cycle occurring in the cylinder at any given moment, as described in further detail below. The cylinder valve mechanism opens to admit air into the interior of cylinder **210** for compression by pistons **120** and **130**, and also opens to eject combustion exhaust from the cylinder interior after combustion has taken place. In addition, in the manner described below, cam surfaces formed in associated sleeves **910** and **910'** actuate the valve mechanisms associated with each of cylinder apertures **210a** and **210b**.

Referring now to FIGS. **4-7**, each valve mechanism for embodiments of the opposed piston diesel engine described herein essentially comprises a single poppet type valve opening into the common combustion chamber between the two opposed pistons in each cylinder pair. The arrangement shown is similar to embodiments of a valve mechanism described in U.S. Publication No. 2009/0173299, incorporated herein by reference. The engine configuration to which the poppet valve mechanism is adapted includes a valve rotatably coupled to the stationary cylinder, and the rotating sleeves surrounding each cylinder. The valve is pivotally attached at one side or end thereof to the edge of the valve port of the cylinder surrounding the pistons, and is actuated by an arm or arms having guides (rollers, etc.) at the distal end(s) thereof, which are captured in corresponding cam track(s) or channel(s) formed in the rotating sleeves.

The engine and valve system operate by gearing or otherwise driving the rotation of the sleeves to correspond with the reciprocation of the pistons of each pair. The cylinder valve ports extend about a portion of the circumferential periphery thereof and are aligned with intake and exhaust runners as previously described, with a single valve disposed across or over each port. As the sleeves rotate about the cylinders, guides attached to the valve actuation arms ride along the cam surfaces or tracks formed in the sleeves. The cam track(s) vary in height or radial distance from the center of the cylinder in their path(s) about the cylinder. As the valve guide(s) travel in the variable radius cam track(s), the valve is periodically pushed inwardly toward the center of the cylinder to open the valve port, and alternately lifted away from the inward position to close the valve port of the inner cylinder. The opening and closing of the valve port permits inflow of intake charges and outflow of exhaust gases from the combustion chamber.

Details of the structure and operation of the valve mechanisms are now described with reference to FIGS. **4-7**. FIGS. **4-7** illustrate a portion of only a single one **912'** of the rotary outer sleeves and a single stationary cylinder **212** with a single piston **120** shown therein, in order to simplify the illustrated

mechanism and clarify a valve mechanism in accordance with embodiments of the present invention.

As seen in FIGS. 4-7, in one embodiment, separate valve ports **212a**, **212b** are formed in the cylinder **212** opposite each of the intake manifold and the exhaust manifold, as previously described. The valve ports **212a**, **212b** are located in the inner cylinder approximately medially of each piston pair, i.e., proximate and in fluid communication with the combustion chamber defined by the cylinder **212** and its two opposed pistons **120** and **130**.

In the embodiment shown in FIGS. 4-7, valve mechanisms **42** and **44** used are similar to the cam-actuated valves described in U.S. Application Ser. No. 60/561,353, incorporated herein by reference. These valve mechanisms include valve members that are connected via hinges to the cylinders and which are actuated as described in the incorporated U.S. patent application, by engagement between actuating members, cam following members, and cam channels formed in the rotating sleeves of embodiments of the present invention. Other suitable alternative valve mechanisms may be used.

In the embodiment shown in FIGS. 4-7, each of the valve mechanisms **42** and **44** essentially comprises a curved plate having a combustion chamber face **44** with a curvature closely conforming to the curvature of the internal cylinder wall **40**. Each valve mechanism further includes a back **46** opposite the face **44**, and a sealing periphery **48**. First and second pairs of opposed actuating arms **54** and **55** extend from the back of the valve. The pairs of actuating arms **54** and **55** extend outwardly adjacent to opposite sides of the inner cylinder valve port **38**.

A first valve attachment hinge **50** connects one edge of the valve periphery **48** to actuating arms **54**, while a second valve attachment hinge **51** connects an opposite edge of the valve periphery **48** to actuating arms **55**. Thus, each of the actuating arms is connected to the back of the valve via a hinge or other mechanism permitting relative rotation between the respective arm and the valve back **46**.

Referring again to FIGS. 4-7, each of the actuating arms in pairs **54** and **55** terminates in a distal end having a cam follower mechanism **58** extending therefrom and riding in corresponding cam channels **36** of the sleeves **912**, **912'**. In the embodiment shown, the cam follower mechanism is resiliently attached to the distal end **56** of the actuating arm **54** by a resilient bushing connector **60** or the like that permits limited relative movement between the cam follower mechanism **58** and the actuating arm **54**. This provides allowance for any small tolerance buildups or dimensional changes due to thermal expansion as the engine **100** is operated. The cam follower mechanism includes at least one cam channel roller **62** extending therefrom and riding within a corresponding cam channel **36**.

In the embodiment shown in FIGS. 4-7, the cam follower mechanism **58** is in the form of a "spider" having a series of radially extending arms, with each of the arms having a separate roller **62** extending therefrom. The rollers **62** comprise small roller bearings that ride against the corresponding inner and outer surfaces of the cam channels **36**. As the radius of the cam channels **36** vary around the cylinder **22**, the rollers are forced radially inwardly and outwardly, thereby driving their attached cam follower mechanisms **58** and valve actuating arms **54** inwardly and outwardly to open and close the valve **42**. Other, alternative methods of valve actuation are also contemplated.

As described in greater detail below, the sleeves **912** and **912'** rotate to actuate the valves **42** and **44**, thereby enabling fluid communication between the interior of cylinder **212** and the separate intake and exhaust passages.

Referring to FIGS. 4-7, the rotating sleeve **912'** includes at least one cam channel **36** fanned therein. The cam channel(s) **36** formed in rotating sleeve **912'** have variable radii in order to actuate the valve mechanism during rotation of the outer cylinder, as described in detail further below.

In one embodiment, a single cam channel **36** is provided in sleeve **912'** for guiding the cam follower mechanism **58**. However, in the particular embodiment shown in FIGS. 4-7, it will be understood that a symmetrical valve actuation system of at least two opposed circumferential cam channels **36** in sleeves **912** and **912'** and corresponding symmetrically opposed linkages between the cam channels and the valve, is provided.

FIGS. 4-7 illustrate the sequence of valve operation through essentially one clockwise revolution of the sleeve **912'** about the stationary cylinder **212**. The variable radius cam channel **36** includes a larger radius valve closed portion **36a**, a decreasing radius ramp portion **36b** causing each of valves **42** and **44** to move from a closed to an open position, a relatively smaller radius valve open portion **36c**, and an increasing radius ramp portion **36d** which causes the valves to move from open positions to its closed positions along the larger radius channel portion **36a**.

Operation of the sleeves and valves during the diesel engine cycle is described as follows, with reference to cylinder **212** and associated sleeves **912**, **912'**. It will be understood that the remainder of the sleeves and valves also operate in the manner described.

Referring to FIG. 6, at the beginning of the combustion cycle, exhaust gasses have been purged and the pistons and associated piston caps within cylinder **212** are at top dead center.

FIG. 6 shows a configuration of one sleeve **912'** of the system during an intake stroke of the cycle. As seen in FIG. 6, the sleeve **912'** rotates within the cylinder case **160** in the direction indicated by arrow "A", thereby causing the cam channels engaging the valve actuating mechanism **58** to travel around the circumference of the cylinder **212**. As the sleeve **912'** rotates and the radius of the cam channel **36** with respect to cylinder **212** varies, so does the distance between the valve actuating mechanism **58** and the center of the cylinder **212** as the outer cylinder rotates.

One edge **42a** of the valve **42** is fixed at a substantially constant radius from the center of the cylinder **212** due to the valve hinge mechanism **50** and the movement of cam follower mechanism **58** within cam channels **36**. However, an opposite edge **42b** of valve **42** is forced to open toward the center of the cylinder **212** as the actuating mechanism **58** reaches the smaller radius portion **36c** of the cam channel **36**. This edge of the valve rotates about the hinge mechanism **50**, thereby opening the valve to admit air for compression and combustion through cylinder opening **212a**.

As seen in FIG. 1, sleeves **912** and **912'** are spaced apart. Also, as seen in FIGS. 4-7, a valve is positioned in each of cylinder openings **212a** and **212b** to control fluid flow through the opening, and each valve has cam followers engaging the cam surfaces in each sleeve. Thus, each valve straddles the gap between the sleeves to engage cam surfaces formed in each sleeve.

In FIG. 6, when valve **42** is forced open by rotation of the sleeves **912'** and **912** (not shown in FIG. 6) and corresponding movement of the cam follower mechanism **58** along the cam channels, movement of the pistons in cylinder **212** away from each other causes air to be drawn into the inner cylinder combustion chamber.

When the piston caps **124** and **134** (FIG. 1) are halfway to bottom dead center, the aperture **212a** is completely open and

air has entered the interior of cylinder **212** for compression. By the time the pistons **120** and **130** are at bottom dead center, sleeves **912** and **912'** have rotated in direction "A" to where the cam follower mechanism of valve **42** has engaged larger radius valve closed portions **36a** of sleeves **912** and **912'**, drawing the valve actuating mechanism **58** outwardly away from the center of the cylinder **212**, thereby closing the edge **42b** of the valve **42**. At this point, the compression stroke is commencing. In addition, the cam follower mechanism associated with valve **44** is engaged with larger radius valve closed portions **36a** of sleeves **912** and **912a**. Thus, valve **44** regulating flow between the interior of cylinder **212** and the exhaust runner is closed.

With both of valves **42** and **44** closed, as the pistons **120** and **130** within cylinder **212** are forced to the center of the cylinder, the air in cylinder **212** is compressed between the pistons. When opposed pistons **120** and **130** are at or near their points of closest approach to each other, the air in the combustion chamber has been compressed and is at or near its maximum pre-combustion temperature. At or near this point, fuel is injected into the combustion chamber between the two pistons and ignited by heat from the compressed air, as is known in the art. Injection of fuel into the combustion chamber may be undertaken using any of a variety of known mechanisms and/or methods. At the same time, while pistons **120** and **130** are approaching each other, sleeves **912** and **912'** continue to rotate in conjunction with each other in the direction indicated by arrow "A" of FIG. 6.

Combustion of the fuel produces expanding gases, forcing the opposed pistons in opposite directions. This initiates the power stroke of the engine cycle. It will be seen that, as cam follower mechanism **58** is traveling along the relatively larger radius portion of cam channel **36** during the compression and combustion cycles, valves **42** and **44** are closed during the compression and combustion cycles described above.

During the power stroke, the pistons **120** and **130** move away from each other as the force of the expanding gasses dictates. At the same time, while pistons **120** and **130** are drawing away from each other, sleeves **912** and **912'** continue to rotate in conjunction with each other in the direction indicated by arrow "A" of FIG. 6.

FIG. 7 shows a configuration of the system during an exhaust stroke of the cycle when the opposed pistons in cylinder **212** are approaching each other after completion of the power stroke. As seen in FIG. 7, the sleeves **912** (not shown in FIG. 7) and **912'** rotate within the cylinder case **160** in the direction indicated by arrow "A", thereby causing the cam channels engaging the valve actuating mechanism **58** to travel around the circumference of the cylinder **212**. As the radius of the cam channel **36** with respect to cylinder **212** varies, so does the distance between the valve actuating mechanism **58** and the center of the inner cylinder **22** as the outer cylinder rotates.

As rotation of the sleeves **912**, **912'** continues, the cam follower mechanism associated with valve **44** engages the decreasing radius ramp portion **36b**, then the smaller radius valve open portion **36c**. Edge **44a** of the valve **44** is fixed at a substantially constant radius from the center of the cylinder **212** due to the valve hinge mechanism **50** and the movement of cam follower mechanism **58** within cam channels **36**. However, edge **44b** of valve **44** is forced to open toward the center of the cylinder **212** as the actuating mechanism **58** reaches the smaller radius portion **36c** of the cam channel **36**. This edge of the valve rotates about the hinge mechanism **50**. Thus, when valve **44** is forced open by rotation of the outer cylinder and corresponding movement of the actuating arms along the cam channels, movement of the opposed pistons toward each other

causes combustion products to be ejected from opening **212b** into the exhaust runner. As the piston caps **124** and **134** of the pistons reach top dead center, the valve mechanism associated with aperture **210b** closes, allowing a new cycle to begin.

In other alternative embodiments, types of valves other than the type described above may be employed. For example, spring-loaded poppet valves may be used. These valves may be actuated as previously described, by engagement between cam channels formed in a rotating outer cylinder and actuating members, or by other features formed on the valves.

A glow plug or other chamber heating mechanism may be incorporated into the assembly to heat the combustion chamber, if desired. The engine may also incorporate an electronic control module (ECM) and associated sensors, as known in the art, to perform and/or facilitate engine control functions.

In another embodiment of the present invention, the engine structure described herein is adapted to execute a two-stroke diesel engine cycle. In one example of such a cycle, at the point of closest approach of the opposed pistons to each other, the cylinder contains a volume of highly compressed air. Diesel fuel is injected into the cylinder by the injector and the fuel immediately ignites because of the pressure and heat inside the cylinder. Expanding gases due to combustion of the fuel drive the opposed pistons apart. This is the power stroke of the engine.

As the opposed pistons near the "bottoms" of their respective strokes (i.e., when the spacing between the opposed pistons nears its greatest extent), sleeve **912'** (see FIGS. 6 and 7) has rotated to a point where engagement between cam channel **36** and exhaust valve **44** has opened the exhaust valve, permitting the pressurized gases to exit the cylinder and relieving the pressure within the cylinder.

When the spacing between the opposed pistons reaches its greatest extent, sleeve **912'** has rotated to a point where engagement between cam channel **36** and intake valve **42** has opened the intake valve, permitting pressurized air to fill the cylinder and forcing the remainder of the exhaust gases from the cylinder. Sleeve **912'** then continues to rotate to a point where engagement between cam channel **36** and exhaust valve **44** closes and the pistons start traveling back toward each other and compressing the newly received charge of air. This is the compression stroke of the engine. As the pistons approach each other, the cycle repeats.

From the above description, it can be seen that interaction between the rotating sleeve and cam channel and the cam follower mechanism can be adjusted to execute a two-stroke diesel engine cycle.

In another embodiment, greater flexibility of control over actuation of the valves is provided by adding to each sleeve another, separate cam channel **36'** radially outboard of cam channel **36**, as shown in FIG. 8. In this embodiment, different cam channels **36** and **36'** engage respective ones of valves **42** and **44** so that actuation of each valve becomes independent of the cam channel controlling actuation of the other valve. This enables, for example, the simultaneous opening and closing of the valves while also enabling the valves to remain open or closed for different, independent lengths of time. This would help facilitate, for example, closing of both intake valve **42** and exhaust valve **44** in rapid succession independent of the respective cam channel configurations.

In order to accommodate one or more additional cam channels, the outer diameters of sleeves **912** and **912'** may need to be greater than in sleeves incorporating only a single cam channel. The engine block may be designed to accommodate the larger diameter sleeves. Then, in instances where only a single cam channel is to be employed, one or more annular

spacers (not shown) may be attached to the smaller diameter sleeves along outer surfaces thereof to occupy the space in the engine block that would otherwise be occupied by the larger diameter sleeves. Sleeve bearings or other bearings may be positioned between the spacers and the engine block to facilitate rotation between the spacers and the engine block.

Referring to FIG. 9, in yet another embodiment, independent control of valves **42'** and **44'** is provided by forming cam channels in sleeves **812** and **812'** as previously described, and by coupling a pair of secondary gear trains **818** and **814** to gears **112** (previously described and shown in FIG. 1). Sleeves **812** and **812'** are rotatably mounted on cylinder **210'** as previously described. Also, geared sleeves **824** and **826** are rotatably mounted on cylinder **210'** as previously described. Sleeves **812** and **812'** are coupled to gears **112** as previously described to rotate the cam channels mounted in the sleeves. Secondary gear trains **818** and **814** are positioned in cylinder case **160** in a known manner.

Gear trains **818** and **814** transfer rotational motion of main gears **112** to respective ones of geared sleeves **824** and **826**, which have cam channels formed therein that are complementary to the cam channels formed in sleeves **812** and **812'**. Thus, valve **44'** is actuated in the manner previously described by the movement of its cam follower mechanism along complementary cam channels formed in sleeve **812** and geared sleeve **826**, while valve **42'** is actuated by the movement of its cam follower mechanism along complementary cam channels formed in sleeve **812'** and geared sleeve **824**. Geared sleeve **824** is geared to rotate (via secondary gear train **818**) in conjunction with an associated gear **112** and its associated sleeve **812'** to control rotation of the sleeves **812'** and **824** such that the complementary cam channels formed in sleeves **812'** and **824** operate in conjunction with each other to actuate valve **42'** in the manner previously described. Similarly, geared sleeve **826** is geared to rotate (via secondary gear train **814**) in conjunction with an associated gear **112** and its associated sleeve **812** to control rotation of the sleeves **812** and **826** such that the complementary cam channels formed in sleeves **812** and **826** operate in conjunction with each other to actuate valve **42** in the manner previously described.

One or more intermediate bearings **822** may be provided along the shafts connecting the gears of the secondary gear trains, for supporting the shafts. This arrangement enables independent control of valves **42'** and **44'** while also enabling positioning of the valves anywhere along substantially the entire length of the cylinder **210'**. This flexible positionability provides additional control over the engine cycle.

In the two-stroke cycle embodiments described above, a turbocharger or a supercharger may be coupled to the engine for compressing the intake air in a known manner.

Referring now to FIGS. **10a-10b**, another embodiment of the valve includes a curved plate **401** including a combustion chamber face **444**, a back **446** opposite the face **444**, and a sealing periphery **448** as previously described. A connector **402** is attached to plate **401**, and an actuating member **404** is attached to connector **402**.

In the embodiment shown, the orientation of actuating member **404** is fixed with respect to plate **401** such that the entire sub-assembly comprising plate **401**, connector **402**, and actuating member **404** is rotatable as a unit. In a particular embodiment, connector **402** and actuating member **404** are formed as a single piece.

Referring to FIGS. **10a-10b**, an arm **404a** formed on each end portion of actuating member **404** moves within in a respective cam channel **36** of a corresponding one of rotating sleeves **912**, **912'** during rotation of the sleeves, in a manner similar to that previously described for cam follower mechanism

58. Lubrication may be provided to facilitate relative motion between the cam channel surfaces and the arms **404a**. Any of a number of suitable lubricating mechanisms may be used, for example, graphite impregnation of the arms and/or the cam channels, application of oils or other viscous lubricants, or other lubricating methods may be used.

In another embodiment (not shown), connector **402** is rotatable with respect to actuating member **404** (i.e., the actuating member is mounted within and can rotate within connector **402**).

In the embodiment shown in FIGS. **10a-10b**, an edge of plate **401** is pivotably attached to a hinge mechanism **350** similar to hinge mechanism **50** previously described. Plate **401** rotates about hinge mechanism **350** during actuation of the valve to open and close the valve, as previously described.

In another embodiment (not shown), a portion of plate **401** abut or engages an edge of cylinder aperture **210a** (or **210b**) or an inner surface of the cylinder to form a pivot point for the plate **401** at the point of contact between the plate and the cylinder. Actuation of the valve by motion of actuating member **404** resulting from rotation of the sleeves **912**, **912'** produces rotation of the plate **401** about the pivot point, to open and close the valve.

Actuation of the valve embodiment shown in FIGS. **10a-10b** is similar to actuation of the embodiment shown in FIGS. **4-7**. As sleeves **912**, **912'** rotate, arms **404a** on actuating member **404** ride within respective cam channels **36**, producing motion of the actuating arm and a corresponding rotation of plate **401**, to open and close the valve.

In yet another embodiment (not shown), a pivot member is provided intermediate the actuating member **404** and plate **401**. The pivot member, actuating member, and plate are coupled together so as to form a substantially rigid member. The pivot member is coupled to the cylinder so as to permit rotation of the rigid member about the pivot member and with respect to the cylinder. In this embodiment, engagement between the actuating member and the cam channel surfaces produces rotation of the rigid member (including the plate **401** seated in the valve aperture) about the pivoting member, to open and close the valve.

In other alternative embodiments, types of valves other than the type described above may be employed. For example, spring-loaded poppet valves may be used. These valves may be actuated as previously described, by engagement between cam channels formed in a rotating outer cylinder and actuating members, or by other features formed on the valves.

The engine may also incorporate an electronic control module (ECM) and associated sensors, as known in the art, to perform and/or facilitate engine control functions.

FIGS. **11-14b** show a cylinder assembly **1100** incorporated into an opposed piston diesel engine including a valve system in accordance with another embodiment of the present invention. The cylinder assembly embodiment **1100** shown in FIGS. **11-14b** is a four-cycle or four-stroke engine as previously described and while it is illustrated with a single cylinder **1210**, it will be understood in view of the previously described embodiments that the structure and operating principles shown in FIGS. **11-14b** may be applied to any number of cylinders depending on the amount of power desired to be produced by the engine. In addition, the structural arrangements and operating principles described herein may alternatively be applied to a two-stroke engine.

Referring to FIG. **11**, each cylinder **1210** of the engine forms (in conjunction with opposed pistons **1120** and **1130** disposed within the cylinder) a combustion chamber for the air-fuel combustion reaction. In the embodiment shown in

11

FIGS. 11-14*b*, each cylinder is associated with a respective pair of rotating outer sleeves 1910, 1910', (e.g., sleeves 1910 and 1910' are rotatably coupled to cylinder 1210 in FIG. 1 along an exterior thereof). FIG. 11 shows rotating sleeves 1910, 1910' associated with cylinder 1210. An engine block or cylinder case (not shown) of the engine encloses the cylinder assemblies and opposed pistons as previously described. Each sleeve has one or more camming surfaces formed therealong for purposes described in greater detail below. Each cylinder is also associated with a pair of connecting rods 1110, a pair of gears 1112, each being gear connected to an associated one of rods 1110, opposing first and second pistons 1120 and 1130 that are each interconnected with a connecting rod 1113, first and second opposing piston caps (not shown) as previously described, and a pair of bearing caps (not shown) as previously described. Optional first and second opposing cylindrical spacers as previously described (not shown) may be affixed to respective ones of the opposed pistons for purposes described below.

In the embodiment shown in FIGS. 11-14*b*, a bevel gear 1115 is attached to an end of an associated one of rotating sleeves 1910, 1910' and is driven by a mating bevel gear 1117 mounted concentrically with another gear 1111 which is driven by a associated one of gears 1112. In the embodiment shown in FIGS. 11-14*b* the rotational axes of gears 1111/1117 and gears 1112 are substantially parallel; however, other arrangements are also possible. Rotation of bevel gears 1117 produces rotation of mating bevel gears 1115, thereby producing rotation of the sleeves 1910, 1910' attached to the gears 1115. Each associated crankshaft is configured to provide predetermined stroke lengths to the first and second pistons 1120 and 1130 residing within each cylinder, as previously described. The opposed first and second pistons 1120 and 1130 may be of a relatively standard design, and have predetermined lengths and predetermined diameters.

Cylinder 1210 resides within respective outer sleeves 1910, 1910', as shown in FIGS. 11 and 12. Cylinder 1210 is also stationary with respect to the rotating sleeves. The gears 1112, through rotation of associated gears 1111 and 1117, are configured to rotate each associated sleeve at a speed of one half crank speed, and each sleeve has a predetermined length. The sleeves of each pair of sleeves associated with an individual cylinder rotate in conjunction with each other, at the same speed and in the same direction. Sleeve or plain bearings (not shown) or any other suitable bearings may be positioned between the cylinders and their respective sleeves to facilitate rotation of the sleeves with respect to the cylinders. Similarly, if desired sleeve or plain bearings (not shown) or any other suitable bearings may be positioned between the rotating sleeves and the engine block (not shown) to facilitate rotation of the sleeves with respect to the engine block. One source of suitable bearings for this application is GGB Bearings of Thorofare, N.J.

Referring to the arrangement within cylinder 1210 of FIG. 11 as exemplary, optional first and second cylindrical spacers (not shown) as previously described may be affixed to the face of the associated pistons 1120 and 1130. The optional spacers are not necessary but may be utilized to provide correct piston lengths for controlling spacing between the piston faces, thereby providing a means for adjusting the compression ratio and generally providing a predetermined degree of compression for heating intake air to facilitate combustion of a fuel injected or otherwise inserted into the combustion chamber. As with the previously described embodiments, the piston lengths are geometrically determined in accordance with the piston stroke length and the lengths of apertures 12010*a*

12

and 1210*b* (described below) formed in the cylinders through which flow exhaust gases and air for combustion.

Referring again to cylinder 1210 of FIGS. 11-14*b*, first and second piston caps (not shown) as previously described may be attached to faces of associated ones of pistons 1120 and 1130 (or to associated optional cylindrical spacers in an embodiment where spacers are used). As previously described, the piston caps may be formed from a sandwich of two sheets of carbon fiber with a ceramic center. The piston caps which are exposed to the combustion event may be slightly concave in form so that when the two piston caps meet in the center of the cylinder they form a somewhat spherical combustion chamber. Only the ceramic cores of the piston caps may actually come into contact with the stationary cylinder wall.

Each piston should have a length from the tire ring to the cap suitable for keeping the piston rings out of the apertures formed in the cylinders. The optional spacers and piston caps may each have a diameter roughly equal to the interior diameter of the associated cylinder, and may be made of carbon fiber, ceramic, or any other suitable material to aid in minimizing thermal inefficiencies during engine operation. The valve mechanism embodiment and associated elements shown in FIGS. 11-14*b* can operate in an engine block similar to block 160 shown in FIG. 3, in a manner similar to that previously described.

As in previously described embodiments, each of cylinder apertures 1210*a* and 1210*b* is associated with a respective valve mechanism which is actuated responsive to the portion (i.e., intake, compression, power, or exhaust) of the engine cycle occurring in the cylinder at any given moment, as described in further detail below. The cylinder valve mechanism opens to admit air into the interior of cylinder 1210 for compression by pistons 1120 and 1130, and also opens to eject combustion exhaust from the cylinder interior after combustion has taken place. In addition, in the manner described below, cam surfaces residing on associated sleeves 1910 and 1910' actuate the valve mechanisms associated with each of apertures 1210*a* and 1210*b*.

The cam surfaces include any surface that engages an actuating portion of the valve to produce rotation of at least a portion of the valve. Thus, the cam channels shown in FIGS. 6-8 have opposed walls, both of which function as cam surfaces because each of the opposed walls engages a portion of the valve to produce valve rotation. Similarly, in other embodiments described herein, rotation of the valve may be produced by engagement between a portion of the valve and a single cam surface or a cam surface without an opposed wall extending therealong.

In the embodiment shown in FIGS. 11-14*b*, the valve mechanism essentially comprises a single poppet type valve opening into the common combustion chamber between the two opposed pistons in each cylinder pair. As in the previously described embodiments, the engine configuration to which the poppet valve mechanism is adapted includes a valve rotatably coupled to the stationary cylinder, and the rotating sleeves surrounding each cylinder. The valve is pivotally coupled to the associated cylinder and is actuated by an arm or arms formed on (or coupled to) an actuator or guide which slides along one or more cam surfaces provided on an associated one of sleeves 1910 and 1910'.

As in the previously described embodiments, the engine and valve system operate by gearing or otherwise driving the rotation of the sleeves to correspond with the reciprocation of the pistons of each pair. The cylinder valve apertures or ports 1210*a* and 1210*b* extend about a portion of the periphery thereof and are aligned with intake and exhaust runners as

13

previously described, with a single valve disposed across or over each port. As the sleeves rotate about the cylinders, guides attached to the valve actuation arms ride along the cam surfaces or tracks formed in the sleeves. The contours of the cam surfaces or track(s) vary in height or radial distance from the center of the cylinder in their path(s) about the cylinder. As the valve actuators or guides travel along the variable radius cam surfaces or channels, the seatable portion of the valve is periodically pushed inwardly toward the center of the cylinder to open the valve port, and alternately lifted away from the inward position to close the valve port of the cylinder. The opening and closing of the valve port permits inflow of intake charges and outflow of exhaust gases from the combustion chamber.

Details of the structure and operation of the valve mechanisms shown in **11-14b** are now described.

Referring to FIGS. **11-14b**, cylinder **1210** has a pair of apertures or valve ports **1210a** and **1210b** formed therealong and positioned so as to enable fluid communication between an interior of the cylinder and the associated intake and exhaust runners formed in an engine block (not shown). Only the apertures formed along a single cylinder **1210** will be described for simplicity. However, it will be understood that any additional cylinders would incorporate similar features arranged so as to facilitate execution of the diesel engine cycle described herein.

In the embodiment shown in FIGS. **11-14b**, a portion of cylinder **1210** is formed by a valve block **2002** interposed between, and connected to, first and second cylinder portions **2004** and **2006**. The valve block contains the cylinder apertures **1210a** and **1210b** and provides a mounting structure for the valves. The valve block **2002** may be welded or otherwise connected to cylinder portions **2004** and **2006** so as to form substantially gas tight seals between the valve block and cylinder portions. The cylinder portions and valve block combine to form the cylinder **2001** in which the pistons **1120** and **1130** reciprocate and in which the fuel is burned.

Valve block **2002** defines an interior **2008** which forms at least a portion of the cylinder combustion chamber, and a pair of apertures **1210a** and **1210b** through which exhaust gases and air for combustion flow into the combustion chamber. Pistons **1120** and **1130** reach the apexes of their respective strokes in the valve block interior.

An interior surface **2030** of the valve block **2002** may have a diameter substantially equal to the inner diameter of cylinder portions **2004** and **2006**, to provide piston guide surfaces within the valve block that are continuous with the inner surfaces of cylinder portions **2004** and **2006**. This permits the pistons to approach each other as closely as possible, enabling greater control of the piston stroke length and compression ratio. The valve block may also contain grooves or other suitable seating features **2032** for receiving therein a pivot portion **1350** of an associated valve (described in greater detail below). The valve block may be cast and finished machined or fabricated using any other suitable techniques.

Valves **2012** are operatively coupled to valve block **2002** for controlling entry of air into the cylinder and exit of exhaust gases from the cylinder according to the requirements of the engine cycle, as previously described. In the embodiment shown in FIGS. **11-14b**, and with reference to FIG. **13** in particular, each of valves **2012** includes a curved plate **1401** having a combustion chamber face **1444**, a back **1446** opposite the face **1444**, and a sealing periphery **1448** as previously described with regard to other valve embodiments. A stem **1407** connects plate **1401** to a pivot portion **1350** which is pivotably coupled to valve block **2002**. Another stem **1405** connects pivot portion **1350** to a guide or actuator portion

14

1404 which slides along a cam surface **2016** residing on an associated sleeve, in the manner previously described. In the embodiment shown, valve **2012** is structured so that plate **1401**, stem **1407**, pivot portion **1350**, stem **1405**, and actuator **1404** are rotatable or pivotably as a unit about pivot portion **1350**. In a particular embodiment, these elements of valve **2012** are formed as a single piece. Pivot portion **1350** may be rotatably positioned in a groove or other locating feature **2032** formed in valve block **2002**. The valve block **2002** with the valves **2012** rotatably mounted thereon combine to form a valve module, generally designated **2014**.

In a particular embodiment, only one rotating sleeve is coupled to the cylinder to actuate the valve.

In addition, the faces of pistons **1120** and **1130** may be provided with recesses configured to receive curved plate **1401** therein during the apexes of the piston strokes. This permits the valve to be in an open position when the pistons are at or near apexes of their strokes, thereby permitting additional flexibility with regard to compression ratios and engine cycle control.

In one particular embodiment, actuator or guide portion **1404** rides along a cam channel or track (not shown) provided in sleeve **1910**. These cam channels may be similar to the cam channels shown in FIGS. **6-8** as previously described. A valve block groove **2032** in which the pivot portion **1350** is seated may be configured, in conjunction with the reaction forces on the actuator portion **1404** produced by the opposed walls of the cam channel, to keep the pivot portion **1350** seated in the groove during operation of the valve. Alternatively, the pivot portion **1350** may be secured in the groove or other locating feature by one or more retention features or devices applied proximate the opposed ends **1350a**, **1350b** of the pivot portion to rotatably secure the pivot portion to the valve block.

In the embodiment shown in FIGS. **11-14b**, a single cam surface **2016** is formed along the sleeve rather than a cam channel having opposed sides. The valve may be spring loaded to bias the valve toward the closed position, as described below.

FIG. **15** shows a sleeve **1910'** in accordance with an embodiment of the present invention. Sleeve **1910'** has a central opening **1911'** dimensioned to have a diameter substantially equal to an inner diameter of associated cylinder portion **2006** (see FIG. **11**), to effectively serve as an extension of the cylinder portion for receiving cam **1130** therein during operation of the engine. Cam surface **2016** is formed along the sleeve and includes associated ramps **2017** to provide initial and terminal engagement between the cam surface and the valve actuator **1404** (not shown) during rotation of the sleeve **1910'**. As the sleeve rotates, the actuator contacts a ramp **2017** and slides along the ramp, initiating rotation of the valve **2012**. When the actuator reaches the radially outermost position **2016a** of the cam surface, the valve is at maximum rotation in the fully open position.

In a particular embodiment, the valve is biased in the closed position using a spring or other mechanism as described herein, and the actuator is engaged by the cam surface only at a point in the cycle when it is desired to rotate the valve to an open position, and for an amount of time sufficient to hold the valve open for the intake or exhaust segment of the cycle. This minimizes the amount of time the actuator is in contact with the cam surfaces, thereby reducing friction and wear on the mechanism.

The valve **2012** may be biased to the closed position using a cantilever spring, torsion spring, or other suitable type of spring (not shown). Then sliding motion of the valve actuator **1404** along the sleeve cam surface **2016** forces the valve into an open configuration against the forces exerted by the spring.

15

When the cam surface rotates further and disengages from the valve actuator, the spring urges the valve back into a closed position.

The cam surfaces formed along the sleeves can be configured to engage the valve to open the valve, to close the valve, or both. Where engagement with the cam surfaces is used only to open the valve, the valve may be biased in a closed position using spring loading or another suitable method, as described above.

The cylinder and associated valve assembly shown in FIGS. 11 and 12 may be assembled by attaching cylinder portions 2004 and 2006 to valve block 2002 as previously described. Valves 2012 are then mounted on the valve block so as to enable operation of the valves to open and close cylinder apertures 1210a and 1210b. Sleeves 1910, 1910' and their associated bevel gears 1115 are then applied and secured to the outer surfaces of the cylinder portions. Alternatively, sleeves 1910, 1910' and their associated bevel gears 1115 may be applied and secured to the outer surfaces of the cylinder portions prior to attachment of the cylinder portions to the valve block.

Referring to FIGS. 11-14b, during operation, rotation of sleeve 1910 produces sliding motion between actuator 1404 and cam surface 2016. FIGS. 14a and 14b show a cross section of the arrangement of FIGS. 11-13 prior to engagement between cam surface 2016 and actuator 1404 (FIG. 14a) and after engagement between cam surface 2016 and actuator 1404 (FIG. 14b). The arrow on cam surface 2016 shows the direction of rotation of the cam surface with respect to the valve 2012. Engagement and disengagement between the cam surface and the actuator as the cam surface rotates causes the valve 2012 to rotate about pivot portion 1350 to force the sealing periphery 1448 radially inwardly (and, optionally, outwardly) with respect to the central axis of the cylinder. This engages and disengages the sealing periphery 1448 of the valve from the edges of aperture 1210a, thereby opening and closing the valve in accordance with the desired engine cycle, as previously described.

Lubrication may be provided to facilitate relative motion between the cam surfaces and the actuator 1404. Any of a number of suitable lubricating mechanisms may be used. For example, graphite impregnation of the actuator and/or the cam surfaces, application of oils or other viscous lubricants, or other lubricating methods may be used.

The engine may also incorporate an electronic control module (ECM) and associated sensors, as known in the art, to perform and/or facilitate engine control functions.

Also, as previously described herein, each of valves 2012 may be actuated by one or more separate cam surfaces configured for controlling the particular valve. The separate cam surfaces configured for controlling the separate valves may be formed on the same sleeve as previously described with regard to FIG. 8. Alternatively, the separate cam surfaces may be formed on separate sleeves as previously described with regard to FIG. 9.

In the embodiments shown in FIG. 6 and in FIGS. 11-15, a single set of cam surfaces is used to actuate both of valves 42 and 44. FIGS. 16a and 16b show a sleeve 2910' in accordance with an alternative embodiment of the present invention. Sleeve 2910' has a central opening 2911' dimensioned to have a diameter substantially equal to an inner diameter of associated cylinder portion 2006 (see FIG. 11), to effectively serve as an extension of the cylinder portion for receiving cam 1130 therein during operation of the engine. A first cam surface 2016 is formed along the sleeve and includes associated ramps 2017 to provide initial and terminal engagement between the cam surface and a first valve actuator 1404a

16

during rotation of the sleeve 2910'. In addition, a second cam surface 3016 is formed along the sleeve and includes associated ramps 3017 to provide initial and terminal engagement between the cam surface and a second valve actuator 1404b during rotation of the sleeve 2910'. Second cam surface 3016 is spaced radially outwardly from first cam surface 2016.

When the second valve is mounted on the valve block or cylinder, the radial distance of the second valve actuator 1404b from the cylinder center is relatively greater than the radial distance of the first valve actuator 1404a from the cylinder center, to enable the second valve actuator to engage radially outermost cam surface 3016. FIGS. 17a-17b show various embodiments of the valve in which the radial distance of the actuator portion 1404b is greater than the radial distance of the actuator 1404 shown in the valve embodiment shown in FIG. 13, when the valve is mounted on the valve block or cylinder. Also, as seen in FIG. 16b, the width "B" of the second actuating portion 1404a (taken parallel with the axis of the cylinder) is relatively greater than the width "A" of the first actuating portion 1404a.

In combination, the radial spacing apart of the cam surfaces 2016 and 3016 and the location of the second actuating portion 1404b at a greater distance from the cylinder center than first actuating portion 1404a ensure that only first cam surface 2016 engages first actuating portion 1404a and only second cam surface 3016 engages second actuating portion 1404b. In this manner, sleeve 2910' is configured to enable independent control of the valves 2012 as previously described in the portion of the specification relating to FIG. 8. That is, instead of both valves being controlled by the same cam surface (or the same group of cam surfaces formed along a single cam ring), each valve is controlled by its own separate cam surface (or group of cam surfaces).

In another embodiment, instead of mirror-imaged cam surfaces formed along opposed sleeves (such as sleeves 1910 and 1910' in FIG. 11) for actuating the valves 2012, each sleeve may have one or more cam surfaces shaped differently from the cam surface(s) on the opposite sleeve. The locations of the cam surfaces on the sleeves, the radial distances of the valve actuating portions of the valves from the cylinder center, and the widths of the actuating portions may be adjusted as previously described so that a first valve is actuated by a cam surface a first one of sleeves, and a second valve is actuated by the other one of opposed sleeves 1115. In this manner, the sleeves are configured to enable independent control of the valves 2012 as previously described.

In a particular embodiment, additional flexibility of control over the engine cycle may be provided by suitably controlling the gear reductions through gears 1111, 1117, and 1115 so that the sleeves (such as sleeves 1910 and 1910' in FIG. 11) rotate at different rates. This configuration may be combined with the previously described control of separate valves by cam surfaces formed on different sleeves to increase flexibility of engine cycle control.

In addition, any desired number of valves may be mounted on the valve block or cylinder and actuated using one of the methods described herein, depending on the space available for mounting and actuation of the valves.

In another embodiment, the cylinder is a conventional cylinder with a pair of apertures formed therein as previously described, to permit the passage of air and exhaust gases into and out of the cylinder interior. The cylinder may be a single piece. The valve block is a separate piece (or pieces) on which the valves can be rotatably mounted, and which is secured to or about an outer surface of the cylinder in a position enabling valves mounted on the valve block to open and close the cylinder apertures, as previously described.

17

Alternatively, a valve as shown in FIGS. 11-14b may be rotatably secured directly to a cylinder proximate one of the cylinder apertures so as to ensure operation of the valve in accordance with the engine cycle, as previously described. The cylinder may be a single piece. A seat for pivot portion 1350 be formed along (or attached to) an outer surface of the cylinder, and the valve mounted thereon via the pivot portion. The valve may be spring loaded as previously described, and is actuated by engagement with cam channels or cam surfaces formed on rotating sleeves which engage actuating portions of the valve, as previously described.

It will be understood that the foregoing descriptions of the embodiments of the present invention are for illustrative purposes only, and that the various structural and operational features herein disclosed are susceptible to a number of modifications, none of which departs from the spirit and scope of the present invention. The preceding description, therefore, is not meant to limit the scope of the invention. Rather, the scope of the invention is to be determined only by the appended claims and their equivalents.

What is claimed is:

1. A valve mechanism comprising:

a valve structured to be operatively coupled to a non-rotating engine cylinder, so as to be rotatable to a first orientation to seal an opening formed in the cylinder, and so as to be rotatable to a second orientation to unseal the opening; and

at least one cam surface structured to be operatively coupled to the cylinder so as to be rotatable about an exterior of the cylinder to engage the valve so as to produce rotation of the valve.

2. An opposed piston engine including a valve mechanism in accordance with claim 1.

3. The engine of claim 2 wherein the engine is a diesel engine.

4. The valve mechanism of claim 1 further comprising a member structured to be mountable on an exterior of the cylinder so as to be rotatable along the cylinder exterior, and wherein the at least one cam surface is formed on the member.

5. The valve mechanism of claim 4 wherein another at least one cam surface is formed on the member, the other at least one cam surface being structured to engage the valve so as to produce rotation of the valve.

6. The valve mechanism of claim 5 wherein the valve has a first actuator and a second actuator formed thereon, wherein the first actuator is structured to engage the at least one cam surface and not the other at least one cam surface during rotation of the member, and wherein the second actuator is structured to engage the other at least one cam surface and not the at least one cam surface during rotation of the member.

7. The valve mechanism of claim 1 wherein the valve is pivotally attached at one side thereof to an edge of an associated valve port formed in the cylinder.

8. The valve mechanism of claim 4 further comprising another member structured to be mountable on an exterior of the cylinder opposite the member and structured so as to be rotatable along the cylinder exterior to rotate about the cylinder, the other member including at least one other cam surface structured to be operatively coupled to the cylinder so as to be rotatable about the cylinder to engage the valve so as to produce rotation of the valve.

9. The valve mechanism of claim 8 wherein the at least one cam surface is structured to engage the valve so as to produce

18

a rotation of the valve at a first point in time during the engine cycle, and the at least one other cam surface is structured to engage the valve so as to produce a rotation of the valve at a second point in time during the engine cycle, and wherein the second point in time is different from the first point in time.

10. The valve mechanism of claim 8 wherein the member and the other member are structured to enable coupling thereof to the cylinder so as to rotate in conjunction with each other, at the same speed and in the same direction.

11. The valve mechanism of claim 4 wherein the member has gear teeth formed along a surface thereof.

12. The valve mechanism of claim 1 wherein the at least one cam surface is structured so as to vary in radial distance from a central axis of the cylinder along an extent of the at least one cam surface.

13. The valve mechanism of claim 7 wherein the at least one cam surface is structured to contact a follower formed on the valve, and wherein the valve mechanism is structured such that motion of the follower along the at least one cam surface rotates the valve to the first position and to the second position.

14. The valve mechanism of claim 1 wherein the valve is structured to be hingedly connected to the cylinder.

15. The valve mechanism of claim 4 wherein the member is structured such that the at least one cam surface travels around a circumference of the cylinder as the member rotates about an exterior of the cylinder.

16. The valve mechanism of claim 4 further comprising another valve and another member positioned opposite the member and structured to rotate the cylinder, the other member including at least one other cam surface operatively coupled to the cylinder so as to be rotatable about the cylinder to engage the other valve so as to produce rotation of the other valve.

17. The valve mechanism of claim 14 wherein the valve is structured to be connected to the cylinder by a hinge mechanism, and wherein the valve is structured to engage the at least one cam surface so as to produce rotation of the valve about the hinge mechanism.

18. The valve mechanism of claim 1 wherein the valve comprises at least one actuating arm, and a cam follower mechanism coupled to the actuating arm and structured to engage the at least one cam surface so as to produce rotation of the valve.

19. The valve mechanism of claim 5 further comprising another valve and wherein a further at least one cam surface is formed on the member and spaced radially outwardly from both the at least one cam surface and the other at least one cam surface, the further at least one cam surface being structured to engage the other valve so as to produce rotation of the other valve.

20. The valve mechanism of claim 1 wherein the valve includes:

a plate portion having a combustion chamber face;
a pivot portion connected to the plate portion and structured for pivotable coupling to the non-rotating cylinder; and
an actuator portion structured to engage the at least one cam surface during rotation of the at least one cam surface.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 9,249,693 B2
APPLICATION NO. : 12/645287
DATED : February 2, 2016
INVENTOR(S) : Warren et al.

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

In the Specification

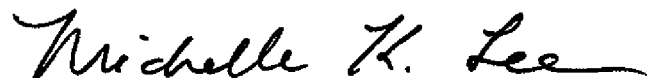
Column 4; Line 9; Please delete "21011" and insert --210b--.

Column 9; Line 28; Please delete "," and insert --.--.

Column 11; Line 23; Please delete "an" and insert --a--.

Column 12; Line 16; Please delete "tire" and insert --fire--.

Signed and Sealed this
Tenth Day of May, 2016



Michelle K. Lee
Director of the United States Patent and Trademark Office